

DECLARATION

I, Koichi OISHI Patent Attorney, of OISHI & PARTNERS, 1-10, Kandasudacho, Chiyoda-ku, Tokyo, Japan, hereby certify that I am the translator of the documents in respect of PCT International Application No. PCT/JP2005/002882 filed on February 23, 2005 and that the following is a true and accurate translation to the best of my knowledge and belief.



Koichi OISHI
Patent Attorney

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[NAME OF DOCUMENT] SPECIFICATION

[TITLE OF THE INVENTION]

CONDUCTIVE PASTE FOR A MULTI-LAYERED CERAMIC
ELECTRONIC COMPONENT AND A METHOD FOR
5 MANUFACTURING A MULTI-LAYERED UNIT FOR A
MULTI-LAYERED CERAMIC ELECTRONIC COMPONENT

[FIELD OF THE INVENTION]

[0001]

10 The present invention relates to a conductive paste for a
multi-layered ceramic electronic component and a method for
manufacturing a multi-layered unit for a multi-layered ceramic electronic
component, and particularly to a conductive paste for a multi-layered
ceramic electronic component which does not dissolve a binder contained
15 in a layer adjacent to an electrode layer of the multi-layered ceramic
electronic component and can reliably prevent short circuit failure from
occurring in a multi-layered ceramic electronic component and a method
for manufacturing a multi-layered unit for a multi-layered ceramic
electronic component which can reliably prevent short circuit failure from
20 occurring in a multi-layered ceramic electronic component.

[BACKGROUND OF THE INVENTION]

[0002]

25 Recently, the need to downsize various electronic devices makes it
necessary to downsize the electronic components incorporated in the
devices and improve the performance thereof. Also in multi-layered
ceramic electronic components, such as multi-layered ceramic capacitors,
it is strongly required to increase the number of layers and make the

laminated unit thinner.

[0003]

When a multi-layered ceramic electronic component as typified by a multi-layered ceramic capacitor is to be manufactured, ceramic powders,
5 a binder such as an acrylic system resin, a butyral resin or the like, a plasticizing agent such as a phthalate ester, glycol, adipate ester, phosphate ester or the like, and an organic solvent such as toluene, methyl ethyl ketone, acetone or the like are mixed and dispersed, thereby preparing a dielectric paste for a ceramic green sheet.

10 [0004]

The dielectric paste is then applied onto a support sheet made of polyethylene terephthalate (PET), polypropylene (PP) or the like using an extrusion coater, a gravure coater or the like to form a coating layer and the coating layer is heated to dryness, thereby fabricating a ceramic green
15 sheet.

[0005]

Further, a conductive powder of nickel or the like and a binder are dissolved into a solvent such as terpineol, thereby preparing a conductive paste and the thus prepared conductive paste is printed on the ceramic
20 green sheet in a predetermined pattern using a screen printing machine and dried, thereby forming an electrode layer.

[0006]

When the electrode layer has been formed, the ceramic green sheet on which the electrode layer is formed is peeled off from the support sheet
25 to form a multi-layered unit including the ceramic green sheet and the electrode layer. Then, a ceramic green chip is formed by laminating a desired number of the multi-layered units to form the laminated body, pressing the laminated body and dicing the laminated body.

[0007]

Finally, the binder is removed from the green chip, the green chip is baked and an external electrode is formed, thereby completing a multi-layered ceramic electronic component such as a multi-layered ceramic capacitor.

[0008]

At present, the need to downsize electronic components and improve the performance thereof makes it necessary to set the thickness of the ceramic green sheet determining the spacing between layers of a multi-layered ceramic capacitor to be equal to or smaller than 3 μm or 2 μm and to laminate three hundred or more multi-layered units each including a ceramic green sheet and an electrode layer.

[DISCLOSURE OF THE INVENTION]

[PROBLEMS TO BE SOLVED BY THE INVENTION]

[0009]

However, in the case where an electrode layer is formed by printing a conductive paste prepared using terpeneol, which is highly popular as a solvent for a conductive paste, on a ceramic green sheet formed using a butyral system resin, which is the most popular binder for a ceramic green sheet, the binder contained in the ceramic green sheet is dissolved by terpeneol contained in the conductive paste and a ceramic green sheet is swollen or partially dissolved, whereby pinholes and cracks are generated in the ceramic green sheet to cause short circuit failure.

[0010]

One proposed solution for these problems is to employ a hydrocarbon system solvent such as kerosene, decane or the like as the solvent for the conductive paste. However, since a hydrocarbon system

solvent such as kerosene, decane or the like does not dissolve the binder component used for the conductive paste, it is impossible to completely replace the conventional solvent such as terpeneol with a hydrocarbon system solvent such as kerosene, decane or the like. Therefore, since the
5 acrylic system resin contained in the ceramic green sheet as a binder is still soluble in the solvent contained in the conductive paste to some extent, it is difficult to prevent generation of pinholes and cracks in the ceramic green sheet in the case where the ceramic green sheet is very thin, and since the viscosity of a hydrocarbon system solvent such as kerosene,
10 decane or the like is lower than that of terpeneol, it is difficult to control the viscosity of the conductive paste.

[0011]

Furthermore, Japanese Patent Application Laid Open No. 5-325633, Japanese Patent Application Laid Open No. 7-21833 and
15 Japanese Patent Application Laid Open No. 7-21832 propose a conductive paste prepared using a hydrogenated terpeneol such as dihydroterpeneol or a terpene system solvent such as dihydroterpeneol acetate instead of terpeneol as a solvent. However, since the acrylic system resin contained in the ceramic green sheet as a binder is also soluble in a hydrogenated
20 terpeneol such as dihydroterpeneol or a terpene system solvent such as dihydroterpeneol acetate to some extent, it is difficult to prevent generation of pinholes and cracks in a ceramic green sheet in the case where the ceramic green sheet is very thin.

[0012]

25 Further, Japanese Patent Application Laid Open No. 2002-270456 discloses a multi-layered ceramic electronic component fabricated by printing a conductive paste containing isobornyl acetate as a solvent, which hardly dissolves a butyral system resin, on a ceramic green sheet

containing a butyral system resin as a binder, thereby forming an electrode layer and discloses that it is preferable to employ ethyl cellulose as a binder of the conductive paste. However, since a conductive paste containing ethyl cellulose as a binder and isobornyl acetate as a solvent
5 has low viscosity and high fluidity, when the conductive paste is printed on a ceramic green sheet using a screen printing machine, the conductive paste leaks from a screen printing plate and the electrode layer cannot be printed in a desired manner. Further, the thus printed electrode layer tends to blot.

10 [0013]

It is therefore an object of the present invention to provide a conductive paste for a multi-layered ceramic electronic component which does not dissolve a binder contained in a layer adjacent to an electrode layer of the multi-layered ceramic electronic component, can reliably
15 prevent short circuit failure from occurring in a multi-layered ceramic electronic component and has excellent printability.

[0014]

It is another object of the present invention to provide a method for manufacturing a multi-layered unit for a multi-layered ceramic electronic
20 component which can reliably prevent short circuit failure from occurring in a multi-layered ceramic electronic component and form an electrode layer in a desired manner.

[MEANS FOR SOLVING THE PROBLEMS]

25 [0015]

The inventors of the present invention vigorously pursued a study for accomplishing the above objects and, as a result, made the discovery that in the case where a conductive paste was prepared using a binder

containing ethyl cellulose having a weight average molecular weight of MW_L and ethyl cellulose having a weight average molecular weight of MW_H at a weight ratio of $X : (1-X)$, where MW_L , MW_H and X were selected so that $X * MW_L + (1-X) * MW_H$ fell within a range of 145,000 to 215,000, and at least one solvent selected from the group consisting of isobornyl acetate, dihydroterpinyl methyl ether, terpinyl methyl ether, α -terpinyl acetate, I-dihydrocarvyl acetate, I-menthone, I-menthyl acetate, I-menthyl acetate, I-perillyl acetate and I-carvyl acetate, it was possible to prepare a conductive paste having a viscosity suitable for printing and dissolve a binder of the conductive paste in a binder in a desired manner and even when the conductive paste was printed on a ceramic green sheet containing an acrylic system resin as a binder, the binder contained in the ceramic green sheet was not dissolved in the solvent contained in the dielectric paste and it was therefore possible to reliably prevent generation of pinholes and cracks in the ceramic green sheet even in the case where the ceramic green sheet was very thin.

[0016]

The present invention is based on these findings and therefore, the objects of the present invention can be accomplished by a conductive paste containing a binder containing ethyl cellulose having a weight average molecular weight of MW_L and ethyl cellulose having a weight average molecular weight of MW_H at a weight ratio of $X : (1-X)$, where MW_L , MW_H and X are selected so that $X * MW_L + (1-X) * MW_H$ falls within a range of 145,000 to 215,000 and at least one solvent selected from the group consisting of isobornyl acetate, dihydroterpinyl methyl ether, terpinyl methyl ether, α -terpinyl acetate, I-dihydrocarvyl acetate, I-menthone, I-menthyl acetate, I-perillyl acetate and I-carvyl acetate.

[0017]

The objects of the present invention can be also accomplished by a method for manufacturing a multi-layered unit for a multi-layered ceramic electronic component comprising a step of printing a conductive paste containing a binder containing ethyl cellulose having a weight
5 average molecular weight of MW_L and ethyl cellulose having a weight average molecular weight of MW_H at a weight ratio of $X : (1-X)$, where MW_L , MW_H and X are selected so that $X * MW_L + (1-X) * MW_H$ falls within a range of 145,000 to 215,000 and at least one solvent selected from the group consisting of isobornyl acetate, dihydroterpinyl methyl ether,
10 terpinyl methyl ether, α -terpinyl acetate, I-dihydrocarvyl acetate, I-menthone, I-menthyl acetate, I-perillyl acetate and I-carvyl acetate on a ceramic green sheet containing a butyral system resin as a binder in a predetermined pattern, thereby forming an electrode layer.

[0018]

15 According to the present invention, it is possible to prepare a conductive paste having a viscosity suitable for printing and form an electrode layer in a desired manner. Further, according to the present invention, even when the conductive paste is printed on a very thin ceramic green sheet containing a butyral system resin as a binder, since
20 the binder contained in the ceramic green sheet is not dissolved in the solvent contained in the dielectric paste, it is possible to reliably prevent the ceramic green sheet from being swollen or partially dissolved and it is therefore possible to reliably prevent generation of pinholes and cracks in the ceramic green sheet even in the case where the ceramic green sheet is
25 very thin.

[0019]

In the present invention, it is preferable for MW_L , MW_H and X to be selected so that $X * MW_L + (1-X) * MW_H$ falls within a range of 155,000

to 205,000.

[0020]

In the present invention, it is preferable for the degree of polymerization of a butyral system resin contained in a ceramic green
5 sheet as a binder to be equal to or larger than 1000.

[0021]

In the present invention, it is preferable for the degree of butyralization of butyral system resin contained in a ceramic green sheet
10 as a binder to be equal to or larger than 64 mol % and equal to or smaller than 78 mol %.

[0022]

In a preferred aspect of the present invention, prior to forming the electrode layer or after forming and drying the electrode layer, a dielectric
paste containing a binder containing ethyl cellulose having a weight
15 average molecular weight of MW_L and ethyl cellulose having a weight average molecular weight of MW_H at a weight ratio of $X : (1-X)$, where MW_L , MW_H and X are selected so that $X * MW_L + (1-X) * MW_H$ falls within a range of 110,000 to 180,000 and at least one solvent selected from the group consisting of isobornyl acetate, dihydroterpinyl methyl ether,
20 terpinyl methyl ether, α -terpinyl acetate, I-dihydrocarvyl acetate, I-menthone, I-menthyl acetate, I-perillyl acetate and I-carvyl acetate is printed on a ceramic green sheet in a complementary pattern to that of the electrode layer, thereby forming a spacer layer.

[0023]

25 According to this preferred aspect of the present invention, since a spacer layer is formed on a ceramic green sheet in a complementary pattern to that of the electrode layer, it is possible to prevent a step from being formed between the surface of the electrode layer and the surface of

the ceramic green sheet where no electrode layer is formed. Therefore, even in the case of laminating a number of multi-layered units each including a ceramic green sheet and an electrode layer and fabricating a multi-layered electronic component such as a multi-layered ceramic capacitor, it is possible to effectively prevent the thus fabricated multi-layered electronic component from being deformed and also effectively prevent delamination of layers from occurring.

[0024]

Further, since a mixed solvent of terpineol and kerosene, dihydroterpineol, terpineol or like, which is popular as a solvent for a dielectric paste for forming a spacer layer, dissolves an acrylic system resin contained in a ceramic green sheet as a binder, when a spacer layer is formed on a ceramic green sheet, the ceramic green sheet is swollen or partially dissolved, whereby voids are generated at the interface between the ceramic green sheet and the spacer layer or fissures or wrinkles are generated on the surface of the spacer layer. As a result, in the case where a multi-layered ceramic capacitor is fabricated by laminating a number of multi-layered units to fabricate a laminated body and baking the laminated body, voids are generated in the multi-layered ceramic capacitor. Further, in the case where fissures or wrinkles are generated on the surface of the spacer layer, since the portions of the spacer layer where fissures or wrinkles are generated tend to drop off, when a number of multi-layered units are laminated to fabricate a laminated body, the portions of the spacer layer where fissures or wrinkles are generated mix into the laminated body as a foreign substance, thereby causing internal defects in the multi-layered ceramic capacitor and generating voids at portions where the spacer layer is missing. However, according to this preferred aspect of the present invention, since a dielectric paste for

forming a spacer layer contains a binder containing ethyl cellulose having a weight average molecular weight of MW_L and ethyl cellulose having a weight average molecular weight of MW_H at a weight ratio of $X : (1-X)$, where MW_L , MW_H and X are selected so that $X * MW_L + (1-X) * MW_H$ falls within a range of 110,000 to 180,000 and at least one solvent selected from the group consisting of isobornyl acetate, dihydroterpinyl methyl ether, terpinyl methyl ether, α -terpinyl acetate, I-dihydrocarvyl acetate, I-menthone, I-menthyl acetate, I-perillyl acetate and I-carvyl acetate and the solvent selected from the group consisting of isobornyl acetate, dihydroterpinyl methyl ether, terpinyl methyl ether, α -terpinyl acetate, I-dihydrocarvyl acetate, I-menthone, I-menthyl acetate, I-perillyl acetate and I-carvyl acetate hardly dissolves an acrylic system resin contained in a ceramic green sheet as a binder, it is possible to reliably prevent the ceramic green sheet from being swollen or partially dissolved so as to generate voids at the interface between the ceramic green sheet and the spacer layer or generate fissures or wrinkles on the surface of the spacer layer, and it is therefore possible to reliably prevent voids from being generated in a multi-layered ceramic electronic component such as a multi-layered ceramic capacitor.

[0025]

Moreover, since a dielectric paste containing a binder containing ethyl cellulose having a weight average molecular weight of MW_L and ethyl cellulose having a weight average molecular weight of MW_H at a weight ratio of $X : (1-X)$, where MW_L , MW_H and X are selected so that $X * MW_L + (1-X) * MW_H$ falls within a range of 110,000 to 180,000 and at least one solvent selected from the group consisting of isobornyl acetate, dihydroterpinyl methyl ether, terpinyl methyl ether, α -terpinyl acetate, I-dihydrocarvyl acetate, I-menthone, I-menthyl acetate, I-perillyl acetate

and I-carvyl acetate has a viscosity suitable for printing, a spacer layer can be formed on a ceramic green sheet in a desired manner by printing a dielectric paste on the ceramic green sheet in a complimentary pattern to that of an electrode layer.

5 [0026]

Further, in a study done by the inventors of the present invention, it was found that in the case of printing a conductive paste on a very thin ceramic green sheet to form an electrode layer, the solvent contained in the conductive paste for forming the electrode layer dissolved or swelled a
10 binder component contained in the ceramic green sheet and, on the other hand, the conductive paste permeated into the ceramic green sheet, thereby causing short circuit failure and that, therefore, it was preferable to form the electrode layer on a support sheet separately from the ceramic green sheet and bond it onto the surface of the ceramic green sheet via an
15 adhesive layer after drying it. However, in the case where the electrode layer is formed on the support sheet separately from the ceramic green sheet in this manner, in order to make the support sheet easy to peel off from the electrode layer, it is preferable to form a release layer containing the same binder as that contained in the ceramic green sheet on the
20 support sheet and print a conductive paste on the release layer, thereby forming an electrode layer. Even in the case of printing a conductive paste on the release layer containing the same binder as that contained in the ceramic green sheet to form an electrode layer, when the release layer contains an acrylic system resin as a binder and the conductive paste
25 contains terpeneol as a solvent, the binder contained in the release layer is dissolved by the solvent contained in the conductive paste so that the release layer is swollen or partially dissolved, whereby voids are generated at the interface between the release layer and the electrode

layer or fissures or wrinkles are generated on the surface of the electrode layer. As a result, in the case where a multi-layered ceramic capacitor is fabricated by laminating a number of multi-layered units to fabricate a laminated body and baking the laminated body, voids are generated in the multi-layered ceramic capacitor. Furthermore, in the case where fissures or wrinkles are generated on the surface of the electrode layer, since the portions of the electrode layer where fissures or wrinkles are generated tend drop off, when a number of multi-layered units are laminated to fabricate a laminated body, the portions of the electrode layer where fissures or wrinkles are generated mix into the laminated body as a foreign substance, thereby causing internal defects in the multi-layered ceramic capacitor and generating voids at portions where the electrode layer was missing.

[0027]

However, according to the present invention, the electrode layer is formed using the conductive paste containing a binder containing ethyl cellulose having a weight average molecular weight of MW_L and ethyl cellulose having a weight average molecular weight of MW_H at a weight ratio of $X : (1-X)$, where MW_L , MW_H and X are selected so that $X * MW_L + (1-X) * MW_H$ falls within a range of 145,000 to 215,000 and at least one solvent selected from the group consisting of isobornyl acetate, dihydroterpinyl methyl ether, terpinyl methyl ether, α -terpinyl acetate, I-dihydrocarvyl acetate, I-menthone, I-menthyl acetate, I-perillyl acetate and I-carvyl acetate and the solvent selected from the group consisting of isobornyl acetate, dihydroterpinyl methyl ether, terpinyl methyl ether, α -terpinyl acetate, I-dihydrocarvyl acetate, I-menthone, I-menthyl acetate, I-perillyl acetate and I-carvyl acetate hardly dissolves the acrylic system resin contained in the ceramic green sheet as a binder. Therefore, even in

the case of forming a release layer containing the same binder as that contained in the ceramic green sheet and printing a conductive paste on the release layer to form an electrode layer it is possible to reliably prevent the release layer from being swollen or partially dissolved so as to generate voids at the interface between the release layer and the electrode layer or generate fissures or wrinkles on the surface of the electrode layer and it is therefore possible to effectively prevent defects from being generated in a multi-layered ceramic electronic component such as a multi-layered ceramic capacitor.

[TECHNICAL ADVANTAGES OF THE INVENTION]

[0028]

According to the present invention, it is possible to provide a conductive paste for a multi-layered ceramic electronic component which does not dissolve a binder contained in a layer adjacent to an electrode layer of the multi-layered ceramic electronic component, can reliably prevent short circuit failure from occurring in a multi-layered ceramic electronic component and has excellent printability.

[0029]

Further, according to the present invention, it is possible to provide a method for manufacturing a multi-layered ceramic electronic component which can reliably prevent short circuit failure from occurring in a multi-layered ceramic electronic component and form an electrode layer in a desired manner.

[DESCRIPTION OF THE PREFERRED EMBODIMENTS]

[0030]

In a preferred embodiment of the present invention, a dielectric

paste for a ceramic green sheet which contains a butyral system resin as a binder is first prepared and is applied onto a long support sheet using an extrusion coater or a wire bar coater, thereby forming a coating layer.

5 A dielectric paste for forming a ceramic green sheet is normally prepared by kneading a dielectric material (ceramic powder) and an organic vehicle obtained by dissolving a butyral system resin into an organic solvent.

[0031]

10 It is preferable for the degree of polymerization of the butyral system resin to be equal to or larger than 1000.

[0032]

Further, it is preferable for the degree of butyralization of butyral system resin to be equal to or larger than 64 mol % and equal to or smaller than 78 mol %.

15 An organic solvent used for preparing the organic vehicle is not particularly limited and an organic solvent such as terpineol, butyl carbitol, acetone, toluene, ethyl acetate and the like can be used for preparing the organic vehicle.

20 The dielectric material can be selected from among various compounds capable of forming a composite oxide or oxide, such as a carbonate, nitrate, hydroxide, organic metallic compound and the like and mixtures thereof. The dielectric material is normally used in the form of a powder whose average particle diameter is about 0.1 μm to about 3.0 μm . The particle diameter of the dielectric raw material is preferably smaller
25 than the thickness of the ceramic green sheet.

The amounts of the respective constituents contained in the dielectric paste is not particularly limited and the dielectric paste may be prepared so as to contain 100 weight parts of a dielectric material, about

2.5 weight part to about 10 weight parts of a butyral system resin and about 50 weight parts to about 320 weight parts of a solvent, for example.

As occasion demands, the dielectric paste may contain additives selected from among various dispersing agents, plasticizing agents, antistatic auxiliary agent, releasing agent, wetting agent and the like. In the case of adding these additives to the dielectric paste, it is preferable to set the total content to be equal to or less than about 10 weight %.

[0033]

As a support sheet coated with the dielectric paste, a polyethylene terephthalate film is employed, for example, and the surface of the support sheet may be coated with a silicon resin, an alkyd resin or the like in order to improve the releasability thereof.

[0034]

The coating layer is then dried at a temperature of about 50 °C to about 100 °C for about 1 to about 20 minutes, whereby a ceramic green sheet is formed on the support sheet.

[0035]

In the present invention, the thickness of the ceramic green sheet after drying is preferably equal to or thinner than 3 μm and more preferably equal to or thinner than 1.5 μm.

[0036]

Next, a conductive paste for forming an electrode layer is printed on the ceramic green sheet formed on the long support sheet in a predetermined pattern using a screen printing machine, a gravure printing machine or the like.

[0037]

It is preferable to form the electrode layer so as to have a dry thickness of about 0.1 μm to about 5 μm and it is more preferable to form

the electrode layer so as to have a dry thickness of about 0.1 μm to about 1.5 μm .

The conductive paste usable for forming an electrode layer is prepared by kneading a conductive material containing any of various
5 conductive metals or alloys, any of various oxides which will form a conductive material containing any of various conductive metals or alloys after baking, an organic metal compound, resinate or the like, and an organic vehicle prepared by dissolving a butyral system resin in an organic solvent.

10 [0038]

In this preferred embodiment of the present invention, the conductive paste contains a binder containing ethyl cellulose having a weight average molecular weight of MW_L and ethyl cellulose having a weight average molecular weight of MW_H at a weight ratio of $X : (1-X)$,
15 where MW_L , MW_H and X are selected so that $X * MW_L + (1-X) * MW_H$ falls within a range of 145,000 to 215,000 and at least one solvent selected from the group consisting of isobornyl acetate, dihydroterpinyl methyl ether, terpinyl methyl ether, α -terpinyl acetate, I-dihydrocarvyl acetate, I-menthone, I-menthyl acetate, I-perillyl acetate and I-carvyl acetate.

20 [0039]

Since the solvent selected from the group consisting of isobornyl acetate, dihydroterpinyl methyl ether, terpinyl methyl ether, α -terpinyl acetate, I-dihydrocarvyl acetate, I-menthone, I-menthyl acetate, I-perillyl acetate and I-carvyl acetate hardly dissolves the butyral system resin
25 contained in a ceramic green sheet as a binder, even in the case of printing the conductive paste on a very thin ceramic green sheet, thereby forming an electrode layer, it is possible to effectively prevent the binder contained in the ceramic green sheet from being dissolved by the solvent

contained in the conductive paste, whereby the ceramic green sheet is swollen or partially dissolved. It is therefore possible to reliably prevent generation of pinholes and cracks in the ceramic green sheet even in the case where the ceramic green sheet is very thin.

5 [0040]

Further, since a conductive paste containing a binder containing ethyl cellulose having a weight average molecular weight of MW_L and ethyl cellulose having a weight average molecular weight of MW_H at a weight ratio of $X : (1-X)$, where MW_L , MW_H and X are selected so that $X * MW_L + (1-X) * MW_H$ falls within a range of 145,000 to 215,000 and at least one solvent selected from the group consisting of isobornyl acetate, dihydroterpinyl methyl ether, terpinyl methyl ether, α -terpinyl acetate, I-dihydrocarvyl acetate, I-menthone, I-menthyl acetate, I-perillyl acetate and I-carvyl acetate has a viscosity suitable for printing, it is possible to print a conductive paste on a ceramic green sheet using a screen printing machine, a gravure printing machine or the like to form an electrode layer in a predetermined pattern in a desired manner.

[0041]

Preferably, MW_L , MW_H and X are selected so that $X * MW_L + (1-X) * MW_H$ falls within a range of 155,000 to 205,000.

As the conductive material used for preparing the conductive paste, Ni, Ni alloy or the mixture thereof is preferably used. The shape of the conductive material is not particularly limited. The conductive material particles may have a spherical shape or a scale-like shape, or the conductive material may contain spherical conductive material particles and scale-like conductive material particles. The average particle diameter of the conductive material is not particularly limited but a conductive material having an average particle diameter of about 0.1 μm

to about 2 μm is normally used for preparing the electrode paste and the conductive material having an average particle diameter of about 0.2 μm to about 1 μm is preferably used for preparing the electrode paste.

The conductive paste preferably contains the binder in an amount
5 about 2.5 weight parts to about 20 weight parts with respect to 100 weight parts of the conductive material.

The content of the solvent is preferably about 20 weight % to about 55 weight % with respect to the weight of the conductive paste.

In order to improve adhesion property, it is preferable for the
10 conductive paste to contain a plasticizing agent. The plasticizing agent contained in the conductive paste is not particularly limited and illustrative examples thereof include phthalate ester, adipic acid, phosphate ester, glycols and the like. The conductive paste contains the plasticizing agent preferably in an amount of about 10 weight % to about
15 300 weight % with respect to 100 weight parts of the binder, more preferably in an amount of about 10 weight parts to about 200 weight parts. In the case where the amount of the plasticizing agent added to the conductive paste is too large, the strength of the electrode layer tends to be markedly lower.

20 As occasion demands, the conductive paste may contain additives selected from among various dispersing agents accessory ingredient compounds and the like.

[0042]

In the present invention, preferably, prior to forming an electrode
25 layer or after forming an electrode layer and drying it, a dielectric paste adapted for forming a spacer layer and containing a binder containing ethyl cellulose having a weight average molecular weight of MW_L and ethyl cellulose having a weight average molecular weight of MW_H at a

weight ratio of $X : (1-X)$, where MW_L , MW_H and X are selected so that $X * MW_L + (1-X) * MW_H$ falls within a range of 110,000 to 180,000 and at least one solvent selected from the group consisting of isobornyl acetate, dihydroterpinyl methyl ether, terpinyl methyl ether, α -terpinyl acetate, I-dihydrocarvyl acetate, I-menthone, I-menthyl acetate, I-perillyl acetate and I-carvyl acetate is printed on the surface of a ceramic green sheet in a complementary pattern to that of the electrode layer using a screen printing machine, a gravure printing machine or the like, thereby forming a spacer layer.

10 [0043]

In the case where a spacer layer is formed on the surface of a ceramic green sheet in a complementary pattern to that of the electrode layer in this manner; it is possible to prevent a step from being formed between the surface of the electrode layer and the surface of the ceramic green sheet where no electrode layer is formed. Therefore, even in the case of laminating a number of multi-layered units each including a ceramic green sheet and an electrode layer and fabricating a multi-layered electronic component such as a multi-layered ceramic capacitor, it is possible to effectively prevent the thus fabricated multi-layered electronic component from being deformed and also effectively prevent delamination of layers from occurring.

[0044]

Furthermore, as described above, since the solvent selected from the group consisting of isobornyl acetate, dihydroterpinyl methyl ether, terpinyl methyl ether, α -terpinyl acetate, I-dihydrocarvyl acetate, I-menthone, I-menthyl acetate, I-perillyl acetate and I-carvyl acetate hardly dissolves the butyral system resin contained in the ceramic green sheet as a binder, it is possible to reliably prevent the ceramic green sheet

from being swollen or partially dissolved so as to generate voids at the interface between the ceramic green sheet and the spacer layer or generate fissures or wrinkles on the surface of the spacer layer.

[0045]

5 Moreover, since the dielectric paste containing a binder containing ethyl cellulose having a weight average molecular weight of MW_L and ethyl cellulose having a weight average molecular weight of MW_H at a weight ratio of $X : (1-X)$, where MW_L , MW_H and X are selected so that $X * MW_L + (1-X) * MW_H$ falls within a range of 110,000 to 180,000 and at least
10 one solvent selected from the group consisting of isobornyl acetate, dihydroterpinyl methyl ether, terpinyl methyl ether, α -terpinyl acetate, I-dihydrocarvyl acetate, I-menthone, I-menthyl acetate, I-perillyl acetate and I-carvyl acetate has a viscosity suitable for printing, a spacer layer can be formed on a ceramic green sheet in a complimentary pattern to
15 that of the electrode layer in a desired manner using a screen printing machine, a gravure printing machine or the like.

In this embodiment, the dielectric paste for forming the spacer layer is prepared in the similar manner to the dielectric paste for forming the ceramic green sheet except that different binder and solvent are used.

20 [0046]

Then, the electrode layer or the electrode layer and the spacer layer are dried and a multi-layered unit including the ceramic green sheet and electrode layer or the electrode layer and the spacer layer laminated on the support sheet is fabricated.

25 [0047]

When a multi-layered ceramic capacitor is to be fabricated, the support sheet is peeled off from the ceramic green sheet of the multi-layered unit and the multi-layered unit is diced to predetermined

dimensions. Then, a predetermined number of the multi-layered units are laminated on the outer layer of a multi-layered ceramic capacitor and the other outer layer of a multi-layered ceramic capacitor is further laminated on the multi-layered units, thereby fabricating a laminated
5 body. Next, the thus obtained laminated body is press molded and diced to predetermined dimensions, thereby fabricating ceramic green chips.

[0048]

The thus fabricated ceramic green chips are placed in a reducing gas atmosphere so that the binder is removed therefrom and the ceramic
10 green chips are baked.

[0049]

Necessary external electrodes are then attached to the thus baked ceramic green chip, thereby manufacturing a multi-layered ceramic capacitor.

15 [0050]

According to this embodiment, since the electrode layer is formed by printing the conductive paste containing a binder containing ethyl cellulose having a weight average molecular weight of MW_L and ethyl cellulose having a weight average molecular weight of MW_H at a weight
20 ratio of $X : (1-X)$, where MW_L , MW_H and X are selected so that $X * MW_L + (1-X) * MW_H$ falls within a range of 145,000 to 215,000 and at least one solvent selected from the group consisting of isobornyl acetate, dihydroterpinyl methyl ether, terpinyl methyl ether, α -terpinyl acetate, I-dihydrocarvyl acetate, I-menthone, I-menthyl acetate, I-perillyl acetate
25 and I-carvyl acetate on the ceramic green sheet containing a butyral system resin as a binder in a predetermined pattern and the solvent selected from the group consisting of isobornyl acetate, dihydroterpinyl methyl ether, terpinyl methyl ether, α -terpinyl acetate, I-dihydrocarvyl

acetate, I-menthone, I-menthyl acetate, I-perillyl acetate and I-carvyl acetate hardly dissolves the butyral system resin contained in a ceramic green sheet as a binder. As a result, even in the case of printing the conductive paste on a very thin ceramic green sheet, thereby forming an electrode layer, it is possible to reliably prevent the binder contained in the ceramic green sheet from being dissolved by the solvent contained in the conductive paste and the ceramic green sheet from being swollen or partially dissolved. Therefore, even in the case where a ceramic green sheet is very thin, it is possible to effectively prevent generation of pinholes or cracks in the ceramic green sheet and it is therefore possible to effectively prevent short circuit failure from occurring in a multi-layered ceramic capacitor fabricated by laminating a number of multi-layered units.

[0051]

Further, according to this embodiment, the spacer layer is formed by printing the dielectric paste containing a binder containing ethyl cellulose having a weight average molecular weight of MW_L and ethyl cellulose having a weight average molecular weight of MW_H at a weight ratio of $X : (1-X)$, where MW_L , MW_H and X are selected so that $X * MW_L + (1-X) * MW_H$ falls within a range of 110,000 to 180,000 and at least one solvent selected from the group consisting of isobornyl acetate, dihydroterpinyl methyl ether, terpinyl methyl ether, α -terpinyl acetate, I-dihydrocarvyl acetate, I-menthone, I-menthyl acetate, I-perillyl acetate and I-carvyl acetate on the ceramic green sheet containing a butyral system resin as a binder in a complementary pattern to that of the electrode layer and the solvent selected from the group consisting of isobornyl acetate, dihydroterpinyl methyl ether, terpinyl methyl ether, α -terpinyl acetate, I-dihydrocarvyl acetate, I-menthone, I-menthyl acetate,

I-perillyl acetate and I-carvyl acetate hardly dissolves the butyral system resin contained in a ceramic green sheet as a binder. As a result, even in the case of printing the dielectric paste on a very thin ceramic green sheet, thereby forming a spacer layer, it is possible to reliably prevent the binder
5 contained in the ceramic green sheet from being dissolved by the solvent contained in the dielectric paste and the ceramic green sheet from being swollen or partially dissolved so as to generate voids at the interface between the ceramic green sheet and the spacer layer or generate fissures or wrinkles on the surface of the spacer layer. Therefore, in the case
10 where a multi-layered ceramic capacitor is fabricated by laminating a number of multi-layered units each including a ceramic green sheet and an electrode layer, it is possible to reliably prevent voids from being generated in the multi-layered ceramic capacitor and it is also possible to reliably prevent the portions of the spacer layer where fissures or
15 wrinkles are generated from dropping off during lamination of a number of the multi-layered units to fabricate the laminated body and mixing into the laminated body as a foreign substance so as to cause internal defects in the multi-layered ceramic capacitor.

[0052]

20 In another preferred embodiment of the present invention, a second support sheet is provided separately from the long support sheet used for forming the ceramic green sheet and the surface of the long second support sheet is coated using a wire bar coater or the like with a dielectric paste containing particles of a dielectric material having
25 substantially the same composition as that of the dielectric material contained in the ceramic green sheet and the same binder as that contained in the ceramic green sheet, thereby forming a coating layer and the coating layer is dried to form a release layer.

[0053]

As the second support sheet, a polyethylene terephthalate film is employed, for example, and the surface of the second support sheet may be coated with a silicon resin, an alkyd resin or the like in order to
5 improve the releasability thereof.

[0054]

The thickness of the release layer is preferably equal to or thinner than that of an electrode layer, more preferably equal to or thinner than about 60 % of the electrode layer thickness and most preferably equal to
10 or thinner than about 30 % of the electrode layer thickness.

[0055]

After the release layer has been dried, the conductive paste for an electrode layer prepared in the above described manner is printed on the surface of the release layer in a predetermined pattern using a screen
15 printing machine, a gravure printing machine or the like, thereby forming an electrode layer.

[0056]

It is preferable to form the electrode layer so as to have a thickness of about 0.1 μm to about 5 μm and it is more preferable to form the
20 electrode layer so as to have a thickness of about 0.1 μm to about 1.5 μm .

[0057]

In this embodiment, the conductive paste contains a binder containing ethyl cellulose having a weight average molecular weight of MW_L and ethyl cellulose having a weight average molecular weight of MW_H at a weight ratio of $X : (1-X)$, where MW_L , MW_H and X are selected
25 so that $X * MW_L + (1-X) * MW_H$ falls within a range of 145,000 to 215,000 and at least one solvent selected from the group consisting of isobornyl acetate, dihydroterpinyl methyl ether, terpinyl methyl ether, α -terpinyl

acetate, I-dihydrocarvyl acetate, I-menthone, I-menthyl acetate, I-perillyl acetate and I-carvyl acetate.

[0058]

Since the solvent selected from the group consisting of isobornyl acetate, dihydroterpinyl methyl ether, terpinyl methyl ether, α -terpinyl acetate, I-dihydrocarvyl acetate, I-menthone, I-menthyl acetate, I-perillyl acetate and I-carvyl acetate hardly dissolves the butyral system resin contained in a ceramic green sheet as a binder, even in the case of forming a release layer containing the same binder as that of the ceramic green sheet and printing the conductive paste on the release layer to form an electrode layer, it is possible to effectively prevent the release layer from being swollen or partially dissolved so as to generate voids at the interface between the release layer and the electrode layer or generate fissures or wrinkles on the surface of the electrode layer.

15 [0059]

Further, since the conductive paste containing a binder containing ethyl cellulose having a weight average molecular weight of MW_L and ethyl cellulose having a weight average molecular weight of MW_H at a weight ratio of $X : (1-X)$, where MW_L , MW_H and X are selected so that $X * MW_L + (1-X) * MW_H$ falls within a range of 145,000 to 215,000 and at least one solvent selected from the group consisting of isobornyl acetate, dihydroterpinyl methyl ether, terpinyl methyl ether, α -terpinyl acetate, I-dihydrocarvyl acetate, I-menthone, I-menthyl acetate, I-perillyl acetate and I-carvyl acetate has a viscosity suitable for printing, an electrode layer can be formed on the release layer in a predetermined pattern using a screen printing machine, a gravure printing machine or the like in a desired manner.

[0060]

Preferably, MW_L , MW_H and X are selected so that $X * MW_L + (1-X) * MW_H$ falls within a range of 155,000 to 205,000.

[0061]

In the present invention, preferably, prior to forming an electrode
5 layer or after forming an electrode layer and drying it, a dielectric paste
containing a binder containing ethyl cellulose having a weight average
molecular weight of MW_L and ethyl cellulose having a weight average
molecular weight of MW_H at a weight ratio of $X : (1-X)$, where MW_L , MW_H
and X are selected so that $X * MW_L + (1-X) * MW_H$ falls within a range of
10 110,000 to 180,000 and at least one solvent selected from the group
consisting of isobornyl acetate, dihydroterpinyl methyl ether, terpinyl
methyl ether, α -terpinyl acetate, I-dihydrocarvyl acetate, I-menthone,
I-menthyl acetate, I-perillyl acetate and I-carvyl acetate and prepared in
the above described manner is printed on the surface of the release layer
15 in a complementary pattern to that of the electrode layer using a screen
printing machine, a gravure printing machine or the like, thereby forming
a spacer layer.

[0062]

In the case where the spacer layer is formed on the surface of a
20 release layer in a complementary pattern to that of the electrode layer in
this manner, it is possible to prevent a step from being formed between
the surface of the electrode layer and the surface of the release layer
where no electrode layer is formed. Therefore, even in the case of
laminating a number of multi-layered units each including a ceramic
25 green sheet and an electrode layer and fabricating a multi-layered
electronic component such as a multi-layered ceramic capacitor, it is
possible to effectively prevent the thus fabricated multi-layered electronic
component from being deformed and also effectively prevent delamination

of layers from occurring.

[0063]

Further, as described above, since the solvent selected from the group consisting of isobornyl acetate, dihydroterpinyl methyl ether, terpinyl methyl ether, α -terpinyl acetate, I-dihydrocarvyl acetate, I-menthone, I-menthyl acetate, I-perillyl acetate and I-carvyl acetate hardly dissolves the butyral system resin contained in the ceramic green sheet as a binder, even in the case of forming the release layer containing the same binder as that of the ceramic green sheet and printing a dielectric paste on the release layer to form a spacer layer, it is possible to effectively prevent the release layer from being swollen or partially dissolved so as to generate voids at the interface between the release layer and the spacer layer or generate fissures or wrinkles on the surface of the spacer layer.

[0064]

Further, since the dielectric paste containing a binder containing ethyl cellulose having a weight average molecular weight of MW_L and ethyl cellulose having a weight average molecular weight of MW_H at a weight ratio of $X : (1-X)$, where MW_L , MW_H and X are selected so that $X * MW_L + (1-X) * MW_H$ falls within a range of 110,000 to 180,000 and at least one solvent selected from the group consisting of isobornyl acetate, dihydroterpinyl methyl ether, terpinyl methyl ether, α -terpinyl acetate, I-dihydrocarvyl acetate, I-menthone, I-menthyl acetate, I-perillyl acetate and I-carvyl acetate has a viscosity suitable for printing, a spacer layer can be formed on the surface of the release layer in a complementary pattern to that of the electrode layer using a screen printing machine, a gravure printing machine or the like in a desired manner.

[0065]

Furthermore, a long third support sheet is provided and the surface of the third support sheet is coated with an adhesive agent solution using a bar coater, an extrusion coater, a reverse coater, a dip coater, a kiss coater or the like and the coating layer is dried, thereby
5 forming an adhesive layer.

[0066]

It is preferable for the adhesive agent solution to contain a binder belonging to the same group as that the binder contained in the ceramic green sheet belongs to, particles of a dielectric material having
10 substantially the same composition as that of dielectric particles contained in the ceramic green sheet, a plasticizing agent, an antistatic agent and a release agent.

[0067]

It is preferable to form an adhesive layer so as to have a thickness
15 thinner than about 0.3 μm , more preferable to form it so as to have a thickness of about 0.02 μm to about 0.3 μm and particularly preferable to form it so as to have a thickness of about 0.02 μm to about 0.2 μm .

[0068]

The adhesive layer formed on the long third support sheet in this
20 manner is bonded onto the surface of the electrode layer or the surfaces of the electrode layer and the spacer layer formed on the long second support sheet or the surface of the ceramic green sheet formed on the support sheet and the third support sheet then is peeled off from the adhesive layer, whereby the adhesive layer is transferred onto the surface
25 of the electrode layer or the surfaces of the electrode layer and the spacer layer or the surface of the ceramic green sheet.

[0069]

In the case where the adhesive layer is transferred onto the

surface of the electrode layer or the surfaces of the electrode layer and the spacer layer, the ceramic green sheet formed on the long support sheet is bonded onto the adhesive layer and the first support sheet is peeled off from the ceramic green sheet so that the ceramic green sheet is transferred onto the surface of the adhesive layer, thereby fabricating a multi-layered unit including the ceramic green sheet and the electrode layer or the electrode layer and the spacer layer.

[0070]

An adhesive layer is transferred onto the surface of the ceramic green sheet of the thus fabricated multi-layered unit in a similar manner to that of transferring the adhesive layer onto the surface of the electrode layer or the surfaces of the electrode layer and the spacer layer and the multi-layered unit including the adhesive layer transferred onto the surface thereof is diced to predetermined dimensions.

[0071]

Similarly, a predetermined number of multi-layered units each including the adhesive layer transferred onto the surface thereof are fabricated and the predetermined number of multi-layered units are laminated, thereby fabricating a multi-layered block.

[0072]

When a multi-layered block is to be fabricated, the multi-layered unit is first positioned on a support formed of polyethylene terephthalate or the like in such a manner that the adhesive layer transferred onto the surface of the multi-layered unit comes into contact with the support and the multi-layered unit is pressed by a pressing machine or the like, whereby the multi-layered unit is bonded onto the support via the adhesive layer.

[0073]

Afterwards, the second support sheet is peeled off from the release layer and the multi-layered unit is laminated on the support.

[0074]

Then, a new multi-layered unit is positioned on the surface of the release layer of the multi-layered unit laminated on the support in such a manner that an adhesive layer formed on the new multi-layered unit comes into contact with the surface of the release layer and the multi-layered unit is pressed using a pressing machine or the like, whereby the new multi-layered unit is laminated on the surface of the release layer of the multi-layered unit laminated on the support via the adhesive layer. Afterwards, the second support sheet is peeled off from the release layer of the new multi-layered unit.

[0075]

Similar processes are repeated, thereby fabricating a multi-layered block including a predetermined number of the laminated multi-layered units.

[0076]

On the other hand, in the case where the adhesive layer is transferred onto the surface of the ceramic green sheet, the electrode layer or the electrode layer and the spacer layer formed on the second support sheet are bonded onto the adhesive layer and then, the second support sheet is peeled off from the release layer, the electrode layer or the electrode layer and the spacer layer and the release layer are transferred onto the surface of the adhesive layer. Thus, a multi-layered unit including the ceramic green sheet and the electrode layer is fabricated.

[0077]

An adhesive layer is transferred onto the surface of the release

layer of the thus obtained multi-layered unit in a similar manner to that of transferring the adhesive layer onto the surface of the ceramic green sheet and the multi-layered unit including the adhesive layer transferred onto the surface thereof is diced to predetermined dimensions.

5 [0078]

Similarly, a predetermined number of multi-layered units each including the adhesive layer transferred onto the surface thereof are fabricated and the predetermined number of multi-layered units are laminated, thereby fabricating a multi-layered block.

10 [0079]

When a multi-layered block is to be fabricated, the multi-layered unit is first positioned on a support formed of polyethylene terephthalate or the like in such a manner that the adhesive layer transferred onto the surface of the multi-layered unit comes into contact with the support and
15 the multi-layered unit is pressed by a pressing machine or the like, whereby the multi-layered unit is bonded onto the support via the adhesive layer.

[0080]

Afterwards, the support sheet is peeled off from the ceramic green
20 sheet and the multi-layered unit is laminated on the support.

[0081]

Then, a new multi-layered unit is positioned on the surface of the ceramic green sheet of the multi-layered unit laminated on the support in such a manner that an adhesive layer formed on the new multi-layered
25 unit comes into contact with the surface of the ceramic green sheet and the multi-layered unit is pressed using a pressing machine or the like, whereby the new multi-layered unit is laminated on the surface of the ceramic green sheet of the multi-layered unit laminated on the support

via the adhesive layer. Afterwards, the support sheet is peeled off from the release layer of the new multi-layered unit.

[0082]

Similar processes are repeated, thereby fabricating a multi-layered block including a predetermined number of the laminated multi-layered units.

[0083]

The thus fabricated multi-layered block including the predetermined number of the laminated multi-layered units is laminated on the outer layer of a multi-layered ceramic capacitor and the other outer layer of a multi-layered ceramic capacitor is further laminated on the multi-layered block, thereby fabricating a laminated body. Next, the thus obtained laminated body is press molded and diced to predetermined dimensions, thereby fabricating a number of ceramic green chips.

[0084]

The thus fabricated ceramic green chips are placed in a reducing gas atmosphere so that the binder is removed therefrom and the ceramic green chips are baked.

[0085]

Necessary external electrodes are then attached to the thus baked ceramic green chip, thereby manufacturing a multi-layered ceramic capacitor.

[0086]

According to this preferred embodiment, since the electrode layer and the spacer layer formed on the second support sheet are dried and then bonded onto the surface of the ceramic green sheet via the adhesive layer, unlike in the case of printing a conductive paste on the surface of the ceramic green sheet to form an electrode layer and printing a

dielectric paste on the surface of the ceramic green sheet to form a spacer layer, it is possible to prevent the conductive paste and the dielectric paste from permeating into the ceramic green sheet and it is therefore possible to laminate the electrode layer and the spacer layer on the surface of the ceramic green sheet in a desired manner.

[0087]

Furthermore, according to this preferred embodiment, the electrode layer is formed using the conductive paste containing a binder containing ethyl cellulose having a weight average molecular weight of MW_L and ethyl cellulose having a weight average molecular weight of MW_H at a weight ratio of $X : (1-X)$, where MW_L , MW_H and X are selected so that $X * MW_L + (1-X) * MW_H$ falls within a range of 145,000 to 215,000 and at least one solvent selected from the group consisting of isobornyl acetate, dihydroterpinyl methyl ether, terpinyl methyl ether, α -terpinyl acetate, I-dihydrocarvyl acetate, I-menthone, I-menthyl acetate, I-perillyl acetate and I-carvyl acetate and the solvent selected from the group consisting of isobornyl acetate, dihydroterpinyl methyl ether, terpinyl methyl ether, α -terpinyl acetate, I-dihydrocarvyl acetate, I-menthone, I-menthyl acetate, I-perillyl acetate and I-carvyl acetate hardly dissolves a butyral system resin contained in a ceramic green sheet as a binder. As a result, even in the case of forming the release layer containing the same binder as that contained in a ceramic green sheet and printing the conductive paste on the release layer, thereby forming an electrode layer, it is possible to effectively prevent the release layer from being swollen or partially dissolved so as to generate pinholes or cracks in the release layer and effectively prevent defects from being generated in a multi-layered ceramic capacitor.

[0088]

Further, according to this preferred embodiment, the spacer layer is formed using the dielectric paste containing a binder containing ethyl cellulose having a weight average molecular weight of MW_L and ethyl cellulose having a weight average molecular weight of MW_H at a weight ratio of $X : (1-X)$, where MW_L , MW_H and X are selected so that $X * MW_L + (1-X) * MW_H$ falls within a range of 110,000 to 180,000 and at least one solvent selected from the group consisting of isobornyl acetate, dihydroterpinyl methyl ether, terpinyl methyl ether, α -terpinyl acetate, I-dihydrocarvyl acetate, I-menthone, I-menthyl acetate, I-perillyl acetate and I-carvyl acetate and the solvent selected from the group consisting of isobornyl acetate, dihydroterpinyl methyl ether, terpinyl methyl ether, α -terpinyl acetate, I-dihydrocarvyl acetate, I-menthone, I-menthyl acetate, I-perillyl acetate and I-carvyl acetate hardly dissolves a butyral system resin contained in a ceramic green sheet as a binder. As a result, even in the case of forming a release layer containing the same binder as that contained in the ceramic green sheet and printing a dielectric paste on the surface of the release layer, thereby forming a spacer layer, it is possible to effectively prevent the release layer from being swollen or partially dissolved so as to generate voids at the interface between the release layer and the spacer layer or generate fissures or wrinkles on the surface of the spacer layer. Therefore, in the case where a multi-layered ceramic capacitor is fabricated by laminating a number of multi-layered units each including a ceramic green sheet and an electrode layer, it is possible to reliably prevent voids from being generated in the multi-layered ceramic capacitor and it is also possible to reliably prevent the portions of the spacer layer where fissures or wrinkles are generated from dropping off during lamination of a number of the multi-layered units to fabricate the laminated body and mixing into the laminated body as a foreign

substance so as to cause internal defects in the multi-layered ceramic capacitor.

[0089]

Moreover, according to this preferred embodiment, since it is possible to prevent the release layer from being swollen or partially dissolved, thereby changing the release strength between the release layer and the electrode layer and the spacer layer or the release layer and the electrode layer, it is possible to effectively prevent defects from being generated when a multi-layered unit is fabricated.

10 [0090]

In a further preferred embodiment, in the case where the adhesive layer is transferred onto the surface of the electrode layer or the surfaces of the electrode layer and the spacer layer, an adhesive layer is transferred onto the surface of a ceramic green sheet of a multi-layered unit fabricated by laminating a release layer, an electrode layer or an electrode layer and a spacer layer, an adhesive layer and a ceramic green sheet on a long second support sheet and without cutting the multi-layered unit, a release layer of another multi-layered unit fabricated by laminating a ceramic green sheet, an adhesive layer, an electrode layer or an electrode layer and a spacer layer, and the release layer on a long support sheet is bonded onto the adhesive layer and the support sheet is peeled off from the ceramic green sheet, whereby two multi-layered units are laminated on the long second support sheet.

[0091]

25 Then, an adhesive layer formed on a third support sheet is transferred onto the ceramic green sheet located on the side of the surface of the laminated two multi-layered units and a release layer of another multi-layered unit fabricated by laminating a ceramic green sheet, an

adhesive layer, an electrode layer or an electrode layer and a spacer layer, and the release layer on a long support sheet is bonded onto the adhesive layer and the support sheet is peeled off from the release layer.

[0092]

5 Similar processes are repeated, thereby fabricating a multi-layered unit set including a predetermined number of laminated multi-layered units. Further, an adhesive layer formed on the third support sheet is transferred onto the surface of the ceramic green sheet located on the side of the surface of the multi-layered unit set, thereby
10 fabricating a laminated body and the laminated body is diced to predetermined dimensions, thereby fabricating a multi-layered blocks.

[0093]

On the other hand, in the case where the adhesive layer is transferred onto the surface of the ceramic green sheet, an adhesive layer
15 is transferred onto the surface of a release layer of a multi-layered unit fabricated by laminating a ceramic green sheet, an adhesive layer, an electrode layer or an electrode layer and a spacer layer, and the release layer on a long support sheet and without cutting the multi-layered unit, a ceramic green sheet of another multi-layered unit fabricated by
20 laminating a release layer, an electrode layer or an electrode layer and a spacer layer, an adhesive layer and a ceramic green sheet on a long second support sheet is bonded onto the adhesive layer and the second support sheet is peeled off from the release layer, whereby two multi-layered units are laminated on the long second support sheet.

25 [0094]

Then, an adhesive layer formed on a third support sheet is transferred onto the release layer located on the side of the surface of the laminated two multi-layered units and a ceramic green sheet of a

multi-layered unit fabricated by laminating a release layer, an electrode layer or an electrode layer and a spacer layer, an adhesive layer and a ceramic green sheet on a long second support sheet is further laminated on the adhesive layer. Then, the second support sheet is peeled off from
5 the release layer.

[0095]

Similar processes are repeated, thereby fabricating a multi-layered unit set including a predetermined number of laminated multi-layered units. Further, an adhesive layer formed on the third
10 support sheet is transferred onto the surface of the release layer located on the side of the surface of the multi-layered unit set, thereby fabricating a laminated body and the laminated body is diced to predetermined dimensions, thereby fabricating multi-layered blocks.

[0096]

15 A multi-layered ceramic capacitor is fabricated using the thus fabricated multi-layered blocks in the manner of the previous preferred embodiment.

[0097]

According to this preferred embodiment, since the multi-layered
20 units are successively laminated on the long second support sheet or support sheet, thereby fabricating the multi-layered unit set including a predetermined number of multi-layered units and the multi-layered unit set is diced to predetermined dimensions, thereby fabricating multi-layered blocks, it is possible to markedly improve the
25 manufacturing efficiency of the multi-layered blocks in comparison with the case where multi-layered blocks are fabricated by laminating multi-layered units each of which has been diced to predetermined dimensions.

[0098]

In a further preferred embodiment of the present invention, in the case where the adhesive layer is transferred onto the surface of the electrode layer or the surfaces of the electrode layer and the spacer layer, an adhesive layer is transferred onto the surface of a ceramic green sheet of a multi-layered unit fabricated by laminating a release layer, an electrode layer or an electrode layer and a spacer layer, an adhesive layer and a ceramic green sheet on a long second support sheet and without cutting the multi-layered unit, an electrode layer or an electrode layer and a spacer layer formed on the second support sheet are bonded onto the adhesive layer and the second support sheet is peeled off from the release layer, whereby the electrode layer and the spacer layer, and the release layer are transferred onto the surface of the adhesive layer.

[0099]

Then, an adhesive layer formed on a third support sheet is transferred onto the surface of the release layer transferred onto the adhesive layer, a ceramic green sheet formed on the support sheet is bonded onto the adhesive layer and the support sheet is peeled off from the ceramic green sheet, whereby the ceramic green sheet is transferred onto the surface of the adhesive layer.

[0100]

Further, an adhesive layer formed on a third support sheet is transferred onto the surface of the ceramic green sheet transferred onto the surface of the adhesive layer, an electrode layer or an electrode layer and a spacer layer formed on the second support sheet are bonded onto the adhesive layer and the second support sheet is peeled off from the release layer, whereby the electrode layer or the electrode layer and the spacer layer, and the release layer are transferred onto the surface of the

adhesive layer.

[0101]

Similar processes are repeated, thereby fabricating a multi-layered unit set including a predetermined number of laminated multi-layered units. Further, an adhesive layer formed on the third support sheet is transferred onto the surface of the ceramic green sheet located on the side of the surface of the multi-layered unit set, thereby fabricating a laminated body and the laminated body is diced to predetermined dimensions, thereby fabricating multi-layered blocks.

10 [0102]

On the other hand, in the case where the adhesive layer is transferred onto the surface of the ceramic green sheet, an adhesive layer is transferred onto the surface of a release layer of a multi-layered unit fabricated by laminating a ceramic green sheet, an adhesive layer, an electrode layer or an electrode layer and a spacer layer, and the release layer on a long support sheet and without cutting the multi-layered unit, a ceramic green sheet of a support sheet is bonded onto the adhesive layer and the support sheet is peeled off from the ceramic green sheet, whereby the ceramic green sheet is transferred onto the adhesive layer.

20 [0103]

Further, an adhesive layer formed on the third support sheet is transferred onto the ceramic green sheet transferred onto the adhesive layer and an electrode layer or an electrode layer and a spacer layer formed on the second support sheet are bonded onto the adhesive layer. Then, the second support sheet is peeled off from the release layer, whereby the electrode layer or the electrode layer and the spacer layer, and the release layer are transferred onto the surface of the adhesive layer.

[0104]

Furthermore, an adhesive layer formed on the third support sheet is transferred onto the release layer transferred onto the adhesive layer and a ceramic green sheet formed on the support sheet is bonded onto the adhesive layer. Then, the support sheet is peeled off from the ceramic green sheet, whereby the ceramic green sheet is transferred onto the surface of the adhesive layer.

[0105]

Similar processes are repeated, thereby fabricating a multi-layered unit set including a predetermined number of laminated multi-layered units. Further, an adhesive layer is transferred onto the surface of the release layer located on the side of the surface of the multi-layered unit set, thereby fabricating a laminated body and the laminated body is diced to predetermined dimensions, thereby fabricating multi-layered blocks.

[0106]

A multi-layered ceramic green sheet is fabricated using the thus fabricated multi-layered block in the manner of the previous embodiment.

[0107]

According to this preferred embodiment, the transferring of the adhesive layer, the transferring of the electrode layer or the electrode layer and the spacer layer and the release layer, the transferring of the adhesive layer and the transferring of the ceramic green sheet onto the long second support sheet or support sheet are repeated, thereby successively laminating the multi-layered units to fabricate the multi-layered unit set including a predetermined number of multi-layered units and the multi-layered unit set is diced to predetermined dimensions, thereby fabricating multi-layered blocks. As a result, it is possible to

markedly improve the manufacturing efficiency of the multi-layered block in comparison with the case where multi-layered blocks are fabricated by laminating multi-layered units each of which has been diced to predetermined dimensions.

5 [0108]

Hereinafter, working examples and comparative examples will be set out in order to further clarify the advantages of the present invention.

[WORKING EXAMPLES]

10 [0109]

Working Example 1

Preparation of a dielectric paste for forming a ceramic green sheet

1.48 weight parts of (BaCa)SiO₃, 1.01 weight parts of Y₂O₃, 0.72 weight part of MgCO₃, 0.13 weight part of MnO and 0.045 weight part of V₂O₅ were mixed, thereby preparing an additive powder.

[0110]

72.3 weight parts of ethyl alcohol, 72.3 weight parts of propyl alcohol, 25.8 weight parts of xylene and 0.93 weight parts of polyethyleneglycol system dispersing agent were added to 100 weight parts of the thus prepared additive powder to prepare a slurry and the additives contained in the slurry were pulverized.

[0111]

When the additives contained in the slurry were to be pulverized, 11.65 grams of the slurry and 450 grams of ZrO₂ beads having a diameter of 2 mm were charged in a polyethylene vessel having an inner volume of 250 cc and the polyethylene vessel was rotated at the circumferential velocity of 45 m/min for sixteen hours, thereby pulverizing the additive powder to prepare the additive slurry.

[0112]

The median diameter of the additives after pulverization was 0.1 μm .

[0113]

5 Then, 15 weight parts of polyvinyl butyral whose degree of polymerization was 1450 and degree of butyralization was 69 mol % was dissolved into a mixture of 42.5 weight parts of ethyl alcohol and 42.5 weight parts of propyl alcohol at 50 °C, thereby preparing a 15 % organic vehicle solution. Further, a slurry having the composition set out below
10 was mixed with the organic vehicle solution for twenty hours using a ball mill having an inner volume of 500 cc, thereby preparing a dielectric paste. When the slurry was to be mixed with the organic vehicle solution, 330.1 grams of the slurry and 900 grams of ZrO_2 beads having a diameter of 2 mm were charged in the polyethylene vessel and the polyethylene
15 vessel was rotated at the circumferential velocity of 45 m/min.

[0114]

BaTiO_3 powders ("BT-02" (Product Name) manufactured by SAKAI CHEMICAL INDUSTRY CO., LTD.: particle diameter 0.2 μm)

		100 weight parts
20	additive slurry	11.65 weight parts
	ethyl alcohol	35.32 weight parts
	propyl alcohol	35.32 weight parts
	xylene	16.32 weight parts
	benzyl butyl phthalate (plasticizing agent)	2.61 weight parts
25	mineral sprit	7.3 weight parts
	polyethylene glycol system dispersing agent	2.36 weight parts
	imidazoline system antistatic auxiliary agent	0.42 weight parts
	organic vehicle	33.74 weight parts

methylethyl ketone	43.81 weight parts
2-butoxyethyl alcohol	43.81 weight parts

As a polyethylene glycol system dispersing agent, a dispersing agent which was obtained by denaturing polyethylene glycol with aliphatic acid and whose hydrophile-liophile balance (HLB) was 5 to 6 was employed.

[0115]

Formation of a ceramic green sheet

A polyethylene terephthalate film was coated with the thus prepared dielectric paste using a die coater at a coating velocity of 50 m/minutes, thereby forming a coating layer and the thus formed coating layer was dried in a drying furnace whose temperature was held at 80 °C, thereby forming a ceramic green sheet having a thickness of 1 μm.

[0116]

Preparation of a conductive paste for forming an electrode layer

1.48 weight parts of (BaCa)SiO₃, 1.01 weight parts of Y₂O₃, 0.72 weight part of MgCO₃, 0.13 weight part of MnO and 0.045 weight part of V₂O₅ were mixed, thereby preparing an additive powder.

[0117]

150 weight parts of acetone, 104.3 weight parts of isobornyl acetate and 1.5 weight parts of polyethylene glycol system dispersing agent were added to 100 weight parts of the thus prepared additive powder to prepare a slurry and the additives contained in the slurry were pulverized using a pulverizer "LMZ0.6" (Product name) manufactured by Ashizawa Finetech Co., Ltd.

[0118]

When the additives contained in the slurry were to be pulverized,

ZrO₂ beads having a diameter of 0.1 mm were charged into a vessel so as to occupy 80 volume % of the vessel, the vessel was rotated at the circumferential velocity of 14 m/min and the slurry was circulated between the vessel and a slurry tank until holding time of the whole
5 slurry of two liters became 30 minutes, thereby pulverizing the additives contained in the slurry.

[0119]

The median diameter of the additives after pulverization was 0.1 μ m.

10 [0120]

Then, acetone was evaporated using an evaporator and removed from the slurry, thereby preparing an additive paste in which the additives were dispersed in terpeneol. The concentration of the additives contained in the additive paste was 49.3 weight %.

15 [0121]

Then, 8 weight parts of a binder containing ethyl cellulose having a weight average molecular weight (MW_H) of 230,000 and ethyl cellulose having a weight average molecular weight (MW_L) of 130,000 at a weight ratio of 75:25, namely, 8 weight parts of ethyl cellulose having an
20 apparent weight average molecular weight of 205,000 defined as $X \cdot MW_L + (1-X) \cdot MW_H$, was dissolved in 92 weight parts of isobornyl acetate at 70 °C, thereby preparing an 8 % organic vehicle solution. Further, a slurry having the composition set out below was dispersed in the organic vehicle solution for sixteen hours using a ball mill. The dispersing conditions
25 were set so that the amount of charged ZrO₂ having a diameter of 2.0 mm was 30 volume % of the ball mill, the amount of the slurry in the ball mill was 60 volume % and the circumferential velocity of the ball mill was 45 m/min.

[0122]

	nickel powder manufactured by Kawatetsu Industry Co., Ltd. and having a particle diameter of 0.2 μm	100 weight parts
	additive paste	1.77 weight parts
5	BaTiO ₃ powder manufactured by SAKAI CHEMICAL INDUSTRY CO., LTD.	19.14 weight parts
	organic vehicle	56.25 weight parts
	polyethylene glycol system dispersing agent	1.19 weight parts
	isobornyl acetate	32.19 weight parts
10	acetone	56 weight parts

[0123]

Then, acetone was evaporated using a stirring device having an evaporator and a heating mechanism and removed from the slurry, thereby preparing a conductive paste. The concentration of the dielectric material contained in the conductive paste was 47 weight %.

[0124]

The viscosity of the thus obtained conductive paste was measured using a rheometer manufactured by HAAKE Co., Ltd. under conditions of a temperature of 25 °C and shearing velocity of 8 sec⁻¹ and was also measured under conditions of a temperature of 25 °C and shearing velocity of 50 sec⁻¹.

[0125]

As a result, it was found that the viscosity of the conductive paste measured under condition of the shearing velocity of 8 sec⁻¹ was 19.4 Ps·s and that the viscosity of the conductive paste measured under condition of the shearing velocity of 50 sec⁻¹ was 10.4 Ps·s.

[0126]

Formation of an electrode layer and fabrication of a multi-layered unit

The thus prepared conductive paste was printed on the ceramic green sheet using a screen printing machine and dried at 90 °C for five minutes, thereby forming an electrode layer having a thickness of 1 µm. Thus, a multi-layered unit including the ceramic green sheet and the electrode layer laminated on the polyethylene terephthalate film was
5 fabricated.

[0127]

The surface roughness (Ra) of the thus formed electrode layer was measured using the "SURFCORDER (SE-30D)" (Product Name)
10 manufactured by Kosaka Laboratory Ltd. As a result, it was found that the surface roughness (Ra) of the electrode layer was 0.124 µm and that the electrode layer having a high surface smoothness was formed.

[0128]

Fabrication of a ceramic green chip

15 The surface of a polyethylene terephthalate film was coated with the dielectric paste prepared in the above described manner using a die coater, thereby forming a coating layer, and the coating layer was dried, thereby forming a ceramic green sheet having a thickness of 10 µm.

[0129]

20 The thus formed ceramic green sheet was peeled off from the polyethylene terephthalate film and diced. Five of the diced ceramic green sheet units were laminated to form a cover layer having a thickness of 50 µm. Further, the multi-layered unit was peeled off from the polyethylene terephthalate film and diced and fifty of the diced multi-layered units
25 were laminated on the cover layer.

[0130]

Then, the ceramic green sheet having a thickness of 10 µm was peeled off from the polyethylene terephthalate film and diced and five of

the ceramic green sheet units were laminated on the multi-layered units laminated on the cover layer, thereby fabricating a laminated body including the lower cover layer having a thickness of 50 μm , an active layer having a thickness of 100 μm and including the laminated fifty
5 multi-layered units each including the ceramic green sheet having a thickness of 1 μm and the electrode layer having a thickness of 1 μm , and an upper cover layer having a thickness of 50 μm .

[0131]

Further, a pressure of 100 MPa was applied onto the thus
10 fabricated laminated body at 70 °C, thereby press molding the laminated body and the laminated body was diced to predetermined dimensions using a dicing machine, thereby fabricating ceramic green chips.

[0132]

Fabrication of a multi-layered ceramic capacitor sample

15 The thus fabricated ceramic green chip was processed under the following conditions in an air atmosphere to remove the binder.

[0133]

Rate of temperature increase: 50 °C / hour

Holding temperature: 240 °C

20 Holding time period: 8 hours

[0134]

After removing the binder, the ceramic green chip was processed and baked under the following conditions in a mixed gas atmosphere of a nitrogen gas and a hydrogen gas whose temperature was controlled at the
25 dew point 20 °C. The contents of the nitrogen gas and the hydrogen gas contained in the mixed gas were 95 volume % and 5 volume %, respectively.

[0135]

Rate of temperature increase: 300 °C / hour

Holding temperature: 1200 °C

Holding time period: 2 hours

Cooling rate: 300 °C / hour

5 [0136]

The thus baked ceramic green chip was subjected to an annealing treatment under the following conditions in a nitrogen gas atmosphere whose temperature was controlled at the dew point 20 °C.

[0137]

10 Rate of temperature increase: 300 °C / hour

Holding temperature: 1000 °C

Holding time period: 3 hours

Cooling rate: 300 °C / hour

[0138]

15 End surfaces of the thus obtained sintered body were polished by the sandblast and coated with In-Ga alloy, thereby forming a terminal electrode. Thus, a multi-layered ceramic capacitor sample was fabricated.

[0139]

A total of fifty multi-layered ceramic capacitor samples were
20 fabricated in a manner similar to the foregoing.

[0140]

Measurement of a short-circuit failure ratio

The resistance value of each of the thus fabricated multi-layered ceramic capacitor samples was measured using a multi-meter to check
25 whether or not short-circuit failure occurred therein.

[0141]

In the case where the thus measured resistance value was equal to or lower than 100 KΩ, it was judged that short-circuit failure occurred in

the multi-layered ceramic capacitor sample. The number of the ceramic capacitor samples in which short-circuit failure occurred was measured and the ratio of the number of the ceramic capacitor samples in which short-circuit failure occurred to the total number of the fabricated multi-layered ceramic capacitor samples was calculated and defined as the short-circuit failure ratio.

[0142]

As a result, the short-circuit failure ratio of the multi-layered ceramic capacitor samples was found to be 12 %, so that the risk of short-circuit failure could be considered insignificant from the practical viewpoint.

[0143]

Working Example 2

A conductive paste was prepared in the manner of Working Example 1 except that a binder containing ethyl cellulose having a weight average molecular weight (MW_H) of 230,000 and ethyl cellulose having a weight average molecular weight (MW_L) of 130,000 at a weight ratio of 50:50, namely, ethyl cellulose having an apparent weight average molecular weight of 180,000 defined as $X \cdot MW_L + (1-X) \cdot MW_H$, was used and the viscosity of the thus prepared conductive paste was measured under conditions of a temperature of 25 °C and shearing velocity of 8 sec⁻¹ and was also measured under conditions of a temperature of 25 °C and shearing velocity of 50 sec⁻¹.

[0144]

As a result, it was found that the viscosity of the conductive paste measured under condition of the shearing velocity of 8 sec⁻¹ was 15.5 Ps·s and that the viscosity of the conductive paste measured under condition of the shearing velocity of 50 sec⁻¹ was 8.5 Ps·s.

[0145]

Then, the thus prepared conductive paste was printed on a ceramic green sheet fabricated in the manner of Working Example 1 using a screen printing machine, thereby forming an electrode layer having a thickness of 1 μm . Thus, a multi-layered unit including the ceramic green sheet and the electrode layer laminated on the polyethylene terephthalate film was fabricated.

[0146]

The surface roughness (R_a) of the thus formed electrode layer was measured using the "SURFCORDER (SE-30D)" (Product Name) manufactured by Kosaka Laboratory Ltd. in the manner of Working Example 1. As a result, it was found that the surface roughness (R_a) of the electrode layer was 0.089 μm and that the electrode layer having a high surface smoothness was formed.

[0147]

Further, a total of fifty multi-layered ceramic capacitor samples were fabricated and the resistance value of each of the thus fabricated multi-layered ceramic capacitor samples was measured using a multi-meter in a manner of Working Example 1 to check whether or not short-circuit failure occurred therein. As a result, the short-circuit failure ratio of the multi-layered ceramic capacitor samples was found to be 4 %, so that the risk of short-circuit failure could be considered insignificant from the practical viewpoint.

[0148]

Working Example 3

A conductive paste was prepared in the manner of Working Example 1 except that a binder containing ethyl cellulose having a weight average molecular weight (MW_H) of 230,000 and ethyl cellulose having a

weight average molecular weight (MW_L) of 130,000 at a weight ratio of 25:75, namely, ethyl cellulose having an apparent weight average molecular weight of 155,000 defined as $X \cdot MW_L + (1-X) \cdot MW_H$, was used and the viscosity of the thus prepared conductive paste was measured
5 under conditions of a temperature of 25 °C and shearing velocity of 8 sec⁻¹ and was also measured under conditions of a temperature of 25 °C and shearing velocity of 50 sec⁻¹.

[0149]

As a result, it was found that the viscosity of the conductive paste
10 measured under condition of the shearing velocity of 8 sec⁻¹ was 11.2 Ps·s and that the viscosity of the conductive paste measured under condition of the shearing velocity of 50 sec⁻¹ was 6.8 Ps·s.

[0150]

Then, the thus prepared conductive paste was printed on a ceramic
15 green sheet fabricated in the manner of Working Example 1 using a screen printing machine, thereby forming an electrode layer having a thickness of 1 μm. Thus, a multi-layered unit including the ceramic green sheet and the electrode layer laminated on the polyethylene terephthalate film was fabricated.

20 [0151]

The surface roughness (R_a) of the thus formed electrode layer was measured using the "SURFCORDER (SE-30D)" (Product Name) manufactured by Kosaka Laboratory Ltd. in the manner of Working Example 1. As a result, it was found that the surface roughness (R_a) of
25 the electrode layer was 0.065 μm and that the electrode layer having a high surface smoothness was formed.

[0152]

Further, a total of fifty multi-layered ceramic capacitor samples

were fabricated and the resistance value of each of the thus fabricated multi-layered ceramic capacitor samples was measured using a multi-meter in a manner of Working Example 1 to check whether or not short-circuit failure occurred therein. As a result, the short-circuit failure ratio of the multi-layered ceramic capacitor samples was found to be 4 %, so that the risk of short-circuit failure could be considered insignificant from the practical viewpoint.

[0153]

Working Example 4

A conductive paste was prepared in the manner of Working Example 1 except that dihydroterpinyl methyl ether was used as a solvent instead of isobornyl acetate and the viscosity of the thus prepared conductive paste was measured under conditions of a temperature of 25 °C and shearing velocity of 8 sec⁻¹ and was also measured under conditions of a temperature of 25 °C and shearing velocity of 50 sec⁻¹.

[0154]

As a result, it was found that the viscosity of the conductive paste measured under condition of the shearing velocity of 8 sec⁻¹ was 16.1 Ps·s and that the viscosity of the conductive paste measured under condition of the shearing velocity of 50 sec⁻¹ was 9.3 Ps·s.

[0155]

Then, the thus prepared conductive paste was printed on a ceramic green sheet fabricated in the manner of Working Example 1 using a screen printing machine, thereby forming an electrode layer having a thickness of 1 μm. Thus, a multi-layered unit including the ceramic green sheet and the electrode layer laminated on the polyethylene terephthalate film was fabricated.

[0156]

The surface roughness (Ra) of the thus formed electrode layer was measured using the "SURFCORDER (SE-30D)" (Product Name) manufactured by Kosaka Laboratory Ltd. in the manner of Working Example 1. As a result, it was found that the surface roughness (Ra) of the electrode layer was 0.111 μm and that the electrode layer having a high surface smoothness was formed.

[0157]

Further, a total of fifty multi-layered ceramic capacitor samples were fabricated and the resistance value of each of the thus fabricated multi-layered ceramic capacitor samples was measured using a multi-meter in a manner of Working Example 1 to check whether or not short-circuit failure occurred therein. As a result, the short-circuit failure ratio of the multi-layered ceramic capacitor samples was found to be 12 %, so that the risk of short-circuit failure could be considered insignificant from the practical viewpoint.

[0158]

Working Example 5

A conductive paste was prepared in the manner of Working Example 4 except that a binder containing ethyl cellulose having a weight average molecular weight (MW_H) of 230,000 and ethyl cellulose having a weight average molecular weight (MW_L) of 130,000 at a weight ratio of 50:50 was used and the viscosity of the thus prepared conductive paste was measured under conditions of a temperature of 25 °C and shearing velocity of 8 sec^{-1} and was also measured under conditions of a temperature of 25 °C and shearing velocity of 50 sec^{-1} .

[0159]

As a result, it was found that the viscosity of the conductive paste measured under condition of the shearing velocity of 8 sec^{-1} was 12.3 $\text{Ps}\cdot\text{s}$

and that the viscosity of the conductive paste measured under condition of the shearing velocity of 50 sec^{-1} was $7.3 \text{ Ps}\cdot\text{s}$.

[0160]

Then, the thus prepared conductive paste was printed on a ceramic green sheet fabricated in the manner of Working Example 1 using a screen printing machine, thereby forming an electrode layer having a thickness of $1 \text{ }\mu\text{m}$. Thus, a multi-layered unit including the ceramic green sheet and the electrode layer laminated on the polyethylene terephthalate film was fabricated.

10 [0161]

The surface roughness (R_a) of the thus formed electrode layer was measured using the "SURFCORDER (SE-30D)" (Product Name) manufactured by Kosaka Laboratory Ltd. in the manner of Working Example 1. As a result, it was found that the surface roughness (R_a) of the electrode layer was $0.066 \text{ }\mu\text{m}$ and that the electrode layer having a high surface smoothness was formed.

[0162]

Further, a total of fifty multi-layered ceramic capacitor samples were fabricated and the resistance value of each of the thus fabricated multi-layered ceramic capacitor samples was measured using a multi-meter in a manner of Working Example 1 to check whether or not short-circuit failure occurred therein. As a result, the short-circuit failure ratio of the multi-layered ceramic capacitor samples was found to be 12 %, so that the risk of short-circuit failure could be considered insignificant from the practical viewpoint.

25 [0163]

Working Example 6

A conductive paste was prepared in the manner of Working

Example 4 except that a binder containing ethyl cellulose having a weight average molecular weight (MW_H) of 230,000 and ethyl cellulose having a weight average molecular weight (MW_L) of 130,000 at a weight ratio of 25:75 was used and the viscosity of the thus prepared conductive paste
5 was measured under conditions of a temperature of 25 °C and shearing velocity of 8 sec^{-1} and was also measured under conditions of a temperature of 25 °C and shearing velocity of 50 sec^{-1} .

[0164]

As a result, it was found that the viscosity of the conductive paste
10 measured under condition of the shearing velocity of 8 sec^{-1} was 8.6 $\text{Ps}\cdot\text{s}$ and that the viscosity of the conductive paste measured under condition of the shearing velocity of 50 sec^{-1} was 5.3 $\text{Ps}\cdot\text{s}$.

[0165]

Then, the thus prepared conductive paste was printed on a ceramic
15 green sheet fabricated in the manner of Working Example 1 using a screen printing machine, thereby forming an electrode layer having a thickness of 1 μm . Thus, a multi-layered unit including the ceramic green sheet and the electrode layer laminated on the polyethylene terephthalate film was fabricated.

20 [0166]

The surface roughness (R_a) of the thus formed electrode layer was measured using the "SURFCORDER (SE-30D)" (Product Name) manufactured by Kosaka Laboratory Ltd. in the manner of Working Example 1. As a result, it was found that the surface roughness (R_a) of
25 the electrode layer was 0.068 μm and that the electrode layer having a high surface smoothness was formed.

[0167]

Further, a total of fifty multi-layered ceramic capacitor samples

were fabricated and the resistance value of each of the thus fabricated multi-layered ceramic capacitor samples was measured using a multi-meter in a manner of Working Example 1 to check whether or not short-circuit failure occurred therein. As a result, the short-circuit failure ratio of the multi-layered ceramic capacitor samples was found to be 8 %, so that the risk of short-circuit failure could be considered insignificant from the practical viewpoint.

[0168]

Working Example 7

A conductive paste was prepared in the manner of Working Example 1 except that terpinyl methyl ether was used as a solvent instead of isobornyl acetate and the viscosity of the thus prepared conductive paste was measured under conditions of a temperature of 25 °C and shearing velocity of 8 sec⁻¹ and was also measured under conditions of a temperature of 25 °C and shearing velocity of 50 sec⁻¹.

[0169]

As a result, it was found that the viscosity of the conductive paste measured under condition of the shearing velocity of 8 sec⁻¹ was 15.6 Ps·s and that the viscosity of the conductive paste measured under condition of the shearing velocity of 50 sec⁻¹ was 9.0 Ps·s.

[0170]

Then, the thus prepared conductive paste was printed on a ceramic green sheet fabricated in the manner of Working Example 1 using a screen printing machine, thereby forming an electrode layer having a thickness of 1 μm. Thus, a multi-layered unit including the ceramic green sheet and the electrode layer laminated on the polyethylene terephthalate film was fabricated.

[0171]

The surface roughness (Ra) of the thus formed electrode layer was measured using the "SURFCORDER (SE-30D)" (Product Name) manufactured by Kosaka Laboratory Ltd. in the manner of Working Example 1. As a result, it was found that the surface roughness (Ra) of the electrode layer was 0.071 μm and that the electrode layer having a high surface smoothness was formed.

[0172]

Further, a total of fifty multi-layered ceramic capacitor samples were fabricated and the resistance value of each of the thus fabricated multi-layered ceramic capacitor samples was measured using a multi-meter in a manner of Working Example 1 to check whether or not short-circuit failure occurred therein. As a result, the short-circuit failure ratio of the multi-layered ceramic capacitor samples was found to be 12 %, so that the risk of short-circuit failure could be considered insignificant from the practical viewpoint.

[0173]

Working Example 8

A conductive paste was prepared in the manner of Working Example 7 except that a binder containing ethyl cellulose having a weight average molecular weight (MW_H) of 230,000 and ethyl cellulose having a weight average molecular weight (MW_L) of 130,000 at a weight ratio of 50:50 was used as a binder of the conductive paste and the viscosity of the thus prepared conductive paste was measured under conditions of a temperature of 25 °C and shearing velocity of 8 sec^{-1} and was also measured under conditions of a temperature of 25 °C and shearing velocity of 50 sec^{-1} .

[0174]

As a result, it was found that the viscosity of the conductive paste

measured under condition of the shearing velocity of 8 sec^{-1} was $11.7 \text{ Ps}\cdot\text{s}$ and that the viscosity of the conductive paste measured under condition of the shearing velocity of 50 sec^{-1} was $6.6 \text{ Ps}\cdot\text{s}$.

[0175]

5 Then, the thus prepared conductive paste was printed on a ceramic green sheet fabricated in the manner of Working Example 1 using a screen printing machine, thereby forming an electrode layer having a thickness of $1 \text{ }\mu\text{m}$. Thus, a multi-layered unit including the ceramic green sheet and the electrode layer laminated on the polyethylene terephthalate
10 film was fabricated.

[0176]

The surface roughness (Ra) of the thus formed electrode layer was measured using the "SURFCORDER (SE-30D)" (Product Name) manufactured by Kosaka Laboratory Ltd. in the manner of Working
15 Example 1. As a result, it was found that the surface roughness (Ra) of the electrode layer was $0.068 \text{ }\mu\text{m}$ and that the electrode layer having a high surface smoothness was formed.

[0177]

Further, a total of fifty multi-layered ceramic capacitor samples
20 were fabricated and the resistance value of each of the thus fabricated multi-layered ceramic capacitor samples was measured using a multi-meter in a manner of Working Example 1 to check whether or not short-circuit failure occurred therein. As a result, the short-circuit failure ratio of the multi-layered ceramic capacitor samples was found to be 14 %,
25 so that the risk of short-circuit failure could be considered insignificant from the practical viewpoint.

[0178]

Working Example 9

A conductive paste was prepared in the manner of Working Example 7 except that a binder containing ethyl cellulose having a weight average molecular weight (MW_H) of 230,000 and ethyl cellulose having a weight average molecular weight (MW_L) of 130,000 at a weight ratio of 25:75 was used as a binder of the conductive paste and the viscosity of the thus prepared conductive paste was measured under conditions of a temperature of 25 °C and shearing velocity of 8 sec⁻¹ and was also measured under conditions of a temperature of 25 °C and shearing velocity of 50 sec⁻¹.

[0179]

As a result, it was found that the viscosity of the conductive paste measured under condition of the shearing velocity of 8 sec⁻¹ was 8.3 Ps·s and that the viscosity of the conductive paste measured under condition of the shearing velocity of 50 sec⁻¹ was 4.78 Ps·s.

[0180]

Then, the thus prepared conductive paste was printed on a ceramic green sheet fabricated in the manner of Working Example 1 using a screen printing machine, thereby forming an electrode layer having a thickness of 1 μm. Thus, a multi-layered unit including the ceramic green sheet and the electrode layer laminated on the polyethylene terephthalate film was fabricated.

[0181]

The surface roughness (R_a) of the thus formed electrode layer was measured using the "SURFCORDER (SE-30D)" (Product Name) manufactured by Kosaka Laboratory Ltd. in the manner of Working Example 1. As a result, it was found that the surface roughness (R_a) of the electrode layer was 0.066 μm and that the electrode layer having a high surface smoothness was formed.

[0182]

Further, a total of fifty multi-layered ceramic capacitor samples were fabricated and the resistance value of each of the thus fabricated multi-layered ceramic capacitor samples was measured using a multi-meter in a manner of Working Example 1 to check whether or not short-circuit failure occurred therein. As a result, the short-circuit failure ratio of the multi-layered ceramic capacitor samples was found to be 6 %, so that the risk of short-circuit failure could be considered insignificant from the practical viewpoint.

10 [0183]

Working Example 10

A conductive paste was prepared in the manner of Working Example 2 except that α -terpinyl acetate was used as a solvent instead of isobornyl acetate and the viscosity of the thus prepared conductive paste was measured under conditions of a temperature of 25 °C and shearing velocity of 8 sec⁻¹ and was also measured under conditions of a temperature of 25 °C and shearing velocity of 50 sec⁻¹.

[0184]

As a result, it was found that the viscosity of the conductive paste measured under condition of the shearing velocity of 8 sec⁻¹ was 12.0 Ps·s and that the viscosity of the conductive paste measured under condition of the shearing velocity of 50 sec⁻¹ was 5.9 Ps·s.

[0185]

Then, the thus prepared conductive paste was printed on a ceramic green sheet fabricated in the manner of Working Example 1 using a screen printing machine, thereby forming an electrode layer having a thickness of 1 μ m. Thus, a multi-layered unit including the ceramic green sheet and the electrode layer laminated on the polyethylene terephthalate

film was fabricated.

[0186]

The surface roughness (Ra) of the thus formed electrode layer was measured using the "SURFCORDER (SE-30D)" (Product Name) manufactured by Kosaka Laboratory Ltd. in the manner of Working Example 1. As a result, it was found that the surface roughness (Ra) of the electrode layer was 0.061 μm and that the electrode layer having a high surface smoothness was formed.

[0187]

Further, a total of fifty multi-layered ceramic capacitor samples were fabricated and the resistance value of each of the thus fabricated multi-layered ceramic capacitor samples was measured using a multi-meter in a manner of Working Example 1 to check whether or not short-circuit failure occurred therein. As a result, the short-circuit failure ratio of the multi-layered ceramic capacitor samples was found to be 8 %, so that the risk of short-circuit failure could be considered insignificant from the practical viewpoint.

[0188]

Working Example 11

A conductive paste was prepared in the manner of Working Example 2 except that I-dihydrocarvyl acetate was used as a solvent instead of isobornyl acetate and the viscosity of the thus prepared conductive paste was measured under conditions of a temperature of 25 °C and shearing velocity of 8 sec^{-1} and was also measured under conditions of a temperature of 25 °C and shearing velocity of 50 sec^{-1} .

[0189]

As a result, it was found that the viscosity of the conductive paste measured under condition of the shearing velocity of 8 sec^{-1} was 11.5 $\text{Ps}\cdot\text{s}$

and that the viscosity of the conductive paste measured under condition of the shearing velocity of 50 sec^{-1} was $6.6 \text{ Ps}\cdot\text{s}$.

[0190]

Then, the thus prepared conductive paste was printed on a ceramic green sheet fabricated in the manner of Working Example 1 using a screen printing machine, thereby forming an electrode layer having a thickness of $1 \text{ }\mu\text{m}$. Thus, a multi-layered unit including the ceramic green sheet and the electrode layer laminated on the polyethylene terephthalate film was fabricated.

[0191]

The surface roughness (R_a) of the thus formed electrode layer was measured using the "SURFCORDER (SE-30D)" (Product Name) manufactured by Kosaka Laboratory Ltd. in the manner of Working Example 1. As a result, it was found that the surface roughness (R_a) of the electrode layer was $0.072 \text{ }\mu\text{m}$ and that the electrode layer having a high surface smoothness was formed.

[0192]

Further, a total of fifty multi-layered ceramic capacitor samples were fabricated and the resistance value of each of the thus fabricated multi-layered ceramic capacitor samples was measured using a multi-meter in a manner of Working Example 1 to check whether or not short-circuit failure occurred therein. As a result, the short-circuit failure ratio of the multi-layered ceramic capacitor samples was found to be 18 %, so that the risk of short-circuit failure could be considered insignificant from the practical viewpoint.

[0193]

Working Example 12

A conductive paste was prepared in the manner of Working

Example 2 except that I-menthone was used as a solvent instead of isobornyl acetate and the viscosity of the thus prepared conductive paste was measured under conditions of a temperature of 25 °C and shearing velocity of 8 sec⁻¹ and was also measured under conditions of a temperature of 25 °C and shearing velocity of 50 sec⁻¹.

[0194]

As a result, it was found that the viscosity of the conductive paste measured under condition of the shearing velocity of 8 sec⁻¹ was 12.4 Ps·s and that the viscosity of the conductive paste measured under condition of the shearing velocity of 50 sec⁻¹ was 6.7 Ps·s.

[0195]

Then, the thus prepared conductive paste was printed on a ceramic green sheet fabricated in the manner of Working Example 1 using a screen printing machine, thereby forming an electrode layer having a thickness of 1 μm. Thus, a multi-layered unit including the ceramic green sheet and the electrode layer laminated on the polyethylene terephthalate film was fabricated.

[0196]

The surface roughness (Ra) of the thus formed electrode layer was measured using the "SURFCORDER (SE-30D)" (Product Name) manufactured by Kosaka Laboratory Ltd. in the manner of Working Example 1. As a result, it was found that the surface roughness (Ra) of the electrode layer was 0.061 μm and that the electrode layer having a high surface smoothness was formed.

[0197]

Further, a total of fifty multi-layered ceramic capacitor samples were fabricated and the resistance value of each of the thus fabricated multi-layered ceramic capacitor samples was measured using a

multi-meter in a manner of Working Example 1 to check whether or not short-circuit failure occurred therein. As a result, the short-circuit failure ratio of the multi-layered ceramic capacitor samples was found to be 6 %, so that the risk of short-circuit failure could be considered insignificant
5 from the practical viewpoint.

[0198]

Working Example 13

A conductive paste was prepared in the manner of Working Example 2 except that I-menthyl acetate was used as a solvent instead of isobornyl acetate and the viscosity of the thus prepared conductive paste
10 was measured under conditions of a temperature of 25 °C and shearing velocity of 8 sec⁻¹ and was also measured under conditions of a temperature of 25 °C and shearing velocity of 50 sec⁻¹.

[0199]

As a result, it was found that the viscosity of the conductive paste
15 measured under condition of the shearing velocity of 8 sec⁻¹ was 10.6 Ps·s and that the viscosity of the conductive paste measured under condition of the shearing velocity of 50 sec⁻¹ was 5.8 Ps·s.

[0200]

Then, the thus prepared conductive paste was printed on a ceramic green sheet fabricated in the manner of Working Example 1 using a screen printing machine, thereby forming an electrode layer having a thickness of 1 μm. Thus, a multi-layered unit including the ceramic green sheet and the electrode layer laminated on the polyethylene terephthalate
20 film was fabricated.

[0201]

The surface roughness (Ra) of the thus formed electrode layer was measured using the "SURFCORDER (SE-30D)" (Product Name)

manufactured by Kosaka Laboratory Ltd. in the manner of Working Example 1. As a result, it was found that the surface roughness (Ra) of the electrode layer was 0.059 μm and that the electrode layer having a high surface smoothness was formed.

5 [0202]

Further, a total of fifty multi-layered ceramic capacitor samples were fabricated and the resistance value of each of the thus fabricated multi-layered ceramic capacitor samples was measured using a multi-meter in a manner of Working Example 1 to check whether or not
10 short-circuit failure occurred therein. As a result, the short-circuit failure ratio of the multi-layered ceramic capacitor samples was found to be 14 %, so that the risk of short-circuit failure could be considered insignificant from the practical viewpoint.

[0203]

15 Working Example 14

A conductive paste was prepared in the manner of Working Example 2 except that I-perillyl acetate was used as a solvent instead of isobornyl acetate and the viscosity of the thus prepared conductive paste was measured under conditions of a temperature of 25 °C and shearing
20 velocity of 8 sec^{-1} and was also measured under conditions of a temperature of 25 °C and shearing velocity of 50 sec^{-1} .

[0204]

As a result, it was found that the viscosity of the conductive paste measured under condition of the shearing velocity of 8 sec^{-1} was 11.8 $\text{Ps}\cdot\text{s}$
25 and that the viscosity of the conductive paste measured under condition of the shearing velocity of 50 sec^{-1} was 6.1 $\text{Ps}\cdot\text{s}$.

As a result, it was found that the viscosity of the conductive paste measured under condition of the shearing velocity of 8 sec^{-1} was 11.8 $\text{Ps}\cdot\text{s}$

and that the viscosity of the conductive paste measured under condition of the shearing velocity of 50 sec^{-1} was $6.1 \text{ Ps}\cdot\text{s}$.

[0205]

Then, the thus prepared conductive paste was printed on a ceramic green sheet fabricated in the manner of Working Example 1 using a screen printing machine, thereby forming an electrode layer having a thickness of $1 \text{ }\mu\text{m}$. Thus, a multi-layered unit including the ceramic green sheet and the electrode layer laminated on the polyethylene terephthalate film was fabricated.

[0206]

The surface roughness (R_a) of the thus formed electrode layer was measured using the "SURFCORDER (SE-30D)" (Product Name) manufactured by Kosaka Laboratory Ltd. in the manner of Working Example 1. As a result, it was found that the surface roughness (R_a) of the electrode layer was $0.069 \text{ }\mu\text{m}$ and that the electrode layer having a high surface smoothness was formed.

[0207]

Further, a total of fifty multi-layered ceramic capacitor samples were fabricated and the resistance value of each of the thus fabricated multi-layered ceramic capacitor samples was measured using a multi-meter in a manner of Working Example 1 to check whether or not short-circuit failure occurred therein. As a result, the short-circuit failure ratio of the multi-layered ceramic capacitor samples was found to be 12 %, so that the risk of short-circuit failure could be considered insignificant from the practical viewpoint.

[0208]

Working Example 15

A conductive paste was prepared in the manner of Working

Example 2 except that I-carvyl acetate was used as a solvent instead of isobornyl acetate and the viscosity of the thus prepared conductive paste was measured under conditions of a temperature of 25 °C and shearing velocity of 8 sec⁻¹ and was also measured under conditions of a temperature of 25 °C and shearing velocity of 50 sec⁻¹.

[0209]

As a result, it was found that the viscosity of the conductive paste measured under condition of the shearing velocity of 8 sec⁻¹ was 10.9 Ps·s and that the viscosity of the conductive paste measured under condition of the shearing velocity of 50 sec⁻¹ was 5.9 Ps·s.

[0210]

Then, the thus prepared conductive paste was printed on a ceramic green sheet fabricated in the manner of Working Example 1 using a screen printing machine, thereby forming an electrode layer having a thickness of 1 μm. Thus, a multi-layered unit including the ceramic green sheet and the electrode layer laminated on the polyethylene terephthalate film was fabricated.

[0211]

The surface roughness (Ra) of the thus formed electrode layer was measured using the "SURFCORDER (SE-30D)" (Product Name) manufactured by Kosaka Laboratory Ltd. in the manner of Working Example 1. As a result, it was found that the surface roughness (Ra) of the electrode layer was 0.059 μm and that the electrode layer having a high surface smoothness was formed.

[0212]

Further, a total of fifty multi-layered ceramic capacitor samples were fabricated and the resistance value of each of the thus fabricated multi-layered ceramic capacitor samples was measured using a

multi-meter in a manner of Working Example 1 to check whether or not short-circuit failure occurred therein. As a result, the short-circuit failure ratio of the multi-layered ceramic capacitor samples was found to be 8 %, so that the risk of short-circuit failure could be considered insignificant
5 from the practical viewpoint.

Comparative Examples

[0213]

Comparative Example 1

10 A conductive paste was prepared in the manner of Working Example 1 except that ethyl cellulose having a weight average molecular weight of 230,000 was used as a binder of a conductive paste and the viscosity of the thus prepared conductive paste was measured under conditions of a temperature of 25 °C and shearing velocity of 8 sec⁻¹ and
15 was also measured under conditions of a temperature of 25 °C and shearing velocity of 50 sec⁻¹.

[0214]

As a result, it was found that the viscosity of the conductive paste measured under condition of the shearing velocity of 8 sec⁻¹ was 23.2 Ps·s
20 and that the viscosity of the conductive paste measured under condition of the shearing velocity of 50 sec⁻¹ was 12.1 Ps·s.

[0215]

Then, the thus prepared conductive paste was printed on a ceramic green sheet fabricated in the manner of Working Example 1 using a
25 screen printing machine, thereby forming an electrode layer having a thickness of 1 μm. Thus, a multi-layered unit including the ceramic green sheet and the electrode layer laminated on the polyethylene terephthalate film was fabricated.

[0216]

The surface roughness (Ra) of the thus formed electrode layer was measured using the "SURFCORDER (SE-30D)" (Product Name) manufactured by Kosaka Laboratory Ltd. in the manner of Working Example 1. As a result, it was found that the surface roughness (Ra) of the electrode layer was 0.210 μm , that is, the surface roughness of the electrode layer was high, so that an electrode layer having a high surface smoothness could not be formed.

[0217]

It was reasonable to conclude that this was because the viscosity of the conductive paste at the shearing velocity of 50 sec^{-1} was too high to print the conductive paste in a desired manner.

[0218]

Further, a total of fifty multi-layered ceramic capacitor samples were fabricated and the resistance value of each of the thus fabricated multi-layered ceramic capacitor samples was measured using a multi-meter in a manner of Working Example 1 to check whether or not short-circuit failure occurred therein. As a result, the short-circuit failure ratio of the multi-layered ceramic capacitor samples was found to be 36 % and it was found that the short-circuit failure was very high.

[0219]

Comparative Example 2

A conductive paste was prepared in the manner of Working Example 1 except that ethyl cellulose having a weight average molecular weight of 130,000 was used as a binder of the conductive paste and the viscosity of the thus prepared conductive paste was measured under conditions of a temperature of 25 $^{\circ}\text{C}$ and shearing velocity of 8 sec^{-1} and was also measured under conditions of a temperature of 25 $^{\circ}\text{C}$ and

shearing velocity of 50 sec⁻¹.

[0220]

As a result, it was found that the viscosity of the conductive paste measured under condition of the shearing velocity of 8 sec⁻¹ was 7.1 Ps·s and that the viscosity of the conductive paste measured under condition of the shearing velocity of 50 sec⁻¹ was 4.7 Ps·s.

[0221]

Then, the thus prepared conductive paste was printed on a ceramic green sheet fabricated in the manner of Working Example 1 using a screen printing machine, thereby forming an electrode layer having a thickness of 1 μm. Thus, a multi-layered unit including the ceramic green sheet and the electrode layer laminated on the polyethylene terephthalate film was fabricated.

[0222]

The surface roughness (Ra) of the thus formed electrode layer was measured using the "SURFCORDER (SE-30D)" (Product Name) manufactured by Kosaka Laboratory Ltd. in the manner of Working Example 1. As a result, it was found that the surface roughness (Ra) of the electrode layer was 0.071 μm, i.e., that the surface smoothness of the electrode layer was high. However, it was found that since the viscosity of the conductive paste at the shearing velocity of 50 sec⁻¹ was too low and the fluidity of the conductive paste was too high, the conductive paste leaked from a screen printing plate and the electrode layer could not be formed in a desired pattern.

[0223]

Comparative Example 3

A dielectric paste for forming a ceramic green sheet was prepared in the manner of Working Example 1 except that butyral system resin

whose degree of polymerization was 800 and degree of butyralization was 69 mol % was used as a binder of the dielectric paste for forming a ceramic green sheet, thereby forming a ceramic green sheet.

Further, a conductive paste was prepared in the manner of Working Example 2 and the viscosity of the thus prepared dielectric paste for forming a ceramic green sheet was measured under conditions of a temperature of 25 °C and shearing velocity of 8 sec⁻¹ and was also measured under conditions of a temperature of 25 °C and shearing velocity of 50 sec⁻¹.

[0224]

As a result, it was found that the viscosity of the conductive paste measured under condition of the shearing velocity of 8 sec⁻¹ was 15.5 Ps·s and that the viscosity of the conductive paste measured under condition of the shearing velocity of 50 sec⁻¹ was 9.8 Ps·s.

[0225]

Then, the thus prepared conductive paste was printed on a ceramic green sheet fabricated in the manner of Working Example 1 using a screen printing machine, thereby forming an electrode layer having a thickness of 1 μm. Thus, a multi-layered unit including the ceramic green sheet and the electrode layer laminated on the polyethylene terephthalate film was fabricated.

[0226]

The surface roughness (Ra) of the thus formed electrode layer was measured using the "SURFCORDER (SE-30D)" (Product Name) manufactured by Kosaka Laboratory Ltd. in the manner of Working Example 1. As a result, it was found that the surface roughness (Ra) of the electrode layer was 0.073 μm and that the electrode layer having a high surface smoothness was formed.

[0227]

Further, a total of fifty multi-layered ceramic capacitor samples were fabricated and the resistance value of each of the thus fabricated multi-layered ceramic capacitor samples was measured using a multi-meter in the manner of Working Example 1 to check whether or not short-circuit failure occurred therein. As a result, the short-circuit failure ratio of the multi-layered ceramic capacitor samples was found to be 30 % and it was found that the short-circuit failure was so high that the samples were of no practical use.

[0228]

Comparative Example 4

A conductive paste was prepared in the manner of Working Example 4 except that ethyl cellulose having a weight average molecular weight of 230,000 was used as a binder of the conductive paste and the viscosity of the thus prepared conductive paste was measured under conditions of a temperature of 25 °C and shearing velocity of 8 sec⁻¹ and was also measured under conditions of a temperature of 25 °C and shearing velocity of 50 sec⁻¹.

[0229]

As a result, it was found that the viscosity of the conductive paste measured under condition of the shearing velocity of 8 sec⁻¹ was 20.3 Ps·s and that the viscosity of the conductive paste measured under condition of the shearing velocity of 50 sec⁻¹ was 11.3 Ps·s.

[0230]

Then, the thus prepared conductive paste was printed on a ceramic green sheet fabricated in the manner of Working Example 1 using a screen printing machine, thereby forming an electrode layer having a thickness of 1 μm. Thus, a multi-layered unit including the ceramic green

sheet and the electrode layer laminated on the polyethylene terephthalate film was fabricated.

[0231]

5 The surface roughness (Ra) of the thus formed electrode layer was measured using the "SURFCORDER (SE-30D)" (Product Name) manufactured by Kosaka Laboratory Ltd. in the manner of Working Example 1. As a result, it was found that the surface roughness (Ra) of the electrode layer was 0.220 μm and that since the surface roughness of the electrode layer was too high, the electrode layer having a high surface
10 smoothness could not be formed.

[0232]

It was reasonable to conclude that this was because the viscosity of the conductive paste at the shearing velocity of 50 sec^{-1} was too high to print the conductive paste in a desired manner.

15 [0233]

Further, a total of fifty multi-layered ceramic capacitor samples were fabricated and the resistance value of each of the thus fabricated multi-layered ceramic capacitor samples was measured using a multi-meter in a manner of Working Example 1 to check whether or not
20 short-circuit failure occurred therein. As a result, the short-circuit failure ratio of the multi-layered ceramic capacitor samples was found to be 34 % and it was found that the short-circuit failure was very high.

[0234]

Comparative Example 5

25 A conductive paste was prepared in the manner of Working Example 4 except that ethyl cellulose having a weight average molecular weight of 130,000 was used as a binder of the conductive paste and the viscosity of the thus prepared conductive paste was measured under

conditions of a temperature of 25 °C and shearing velocity of 8 sec⁻¹ and was also measured under conditions of a temperature of 25 °C and shearing velocity of 50 sec⁻¹.

[0235]

5 As a result, it was found that the viscosity of the conductive paste measured under condition of the shearing velocity of 8 sec⁻¹ was 5.3 Ps·s and that the viscosity of the conductive paste measured under condition of the shearing velocity of 50 sec⁻¹ was 3.2 Ps·s.

[0236]

10 Then, the thus prepared conductive paste was printed on a ceramic green sheet fabricated in the manner of Working Example 1 using a screen printing machine, thereby forming an electrode layer having a thickness of 1 μm. Thus, a multi-layered unit including the ceramic green sheet and the electrode layer laminated on the polyethylene terephthalate
15 film was fabricated.

[0237]

The surface roughness (Ra) of the thus formed electrode layer was measured using the "SURFCORDER (SE-30D)" (Product Name) manufactured by Kosaka Laboratory Ltd. in the manner of Working
20 Example 1. As a result, it was found that the surface roughness (Ra) of the electrode layer was 0.064 μm and that the surface smoothness of the electrode layer was high. However, it was found that since the viscosity of the conductive paste at the shearing velocity of 50 sec⁻¹ was too low and the fluidity of the conductive paste was too high, the conductive paste
25 leaked from a screen printing plate and the electrode layer could not be formed in a desired pattern.

[0238]

Comparative Example 6

A dielectric paste for forming a ceramic green sheet was prepared in the manner of Working Example 1 except that butyral system resin whose degree of polymerization was 800 and degree of butyralization was 69 mol % was used as a binder of the dielectric paste for forming a ceramic green sheet, thereby forming a ceramic green sheet.

Further, a conductive paste was prepared in the manner of Working Example 5 and the viscosity of the thus prepared dielectric paste for forming a ceramic green sheet was measured under conditions of a temperature of 25 °C and shearing velocity of 8 sec⁻¹ and was also measured under conditions of a temperature of 25 °C and shearing velocity of 50 sec⁻¹.

[0239]

As a result, it was found that the viscosity of the conductive paste measured under condition of the shearing velocity of 8 sec⁻¹ was 12.3 Ps·s and that the viscosity of the conductive paste measured under condition of the shearing velocity of 50 sec⁻¹ was 7.3 Ps·s.

[0240]

Then, the thus prepared conductive paste was printed on a ceramic green sheet fabricated in the manner of Working Example 1 using a screen printing machine, thereby forming an electrode layer having a thickness of 1 μm. Thus, a multi-layered unit including the ceramic green sheet and the electrode layer laminated on the polyethylene terephthalate film was fabricated.

[0241]

The surface roughness (Ra) of the thus formed electrode layer was measured using the "SURFCORDER (SE-30D)" (Product Name) manufactured by Kosaka Laboratory Ltd. in the manner of Working Example 1. As a result, it was found that the surface roughness (Ra) of

the electrode layer was 0.078 μm and that the electrode layer having a high surface smoothness was formed.

[0242]

Further, a total of fifty multi-layered ceramic capacitor samples were fabricated and the resistance value of each of the thus fabricated multi-layered ceramic capacitor samples was measured using a multi-meter in a manner of Working Example 1 to check whether or not short-circuit failure occurred therein. As a result, the short-circuit failure ratio of the multi-layered ceramic capacitor samples was found to be 34 % and it was found that the short-circuit failure was so high that the samples were of no practical use.

[0243]

Comparative Example 7

A conductive paste was prepared in the manner of Working Example 7 except that ethyl cellulose having a weight average molecular weight of 230,000 was used as a binder of the conductive paste and the viscosity of the thus prepared conductive paste was measured under conditions of a temperature of 25 °C and shearing velocity of 8 sec^{-1} and was also measured under conditions of a temperature of 25 °C and shearing velocity of 50 sec^{-1} .

[0244]

As a result, it was found that the viscosity of the conductive paste measured under condition of the shearing velocity of 8 sec^{-1} was 21.3 $\text{Ps}\cdot\text{s}$ and that the viscosity of the conductive paste measured under condition of the shearing velocity of 50 sec^{-1} was 11.75 $\text{Ps}\cdot\text{s}$.

As a result, it was found that the viscosity of the conductive paste measured under condition of the shearing velocity of 8 sec^{-1} was 21.3 $\text{Ps}\cdot\text{s}$ and that the viscosity of the conductive paste measured under condition of

the shearing velocity of 50 sec^{-1} was $11.75 \text{ Ps}\cdot\text{s}$.

[0245]

Then, the thus prepared conductive paste was printed on a ceramic green sheet fabricated in the manner of Working Example 1 using a screen printing machine, thereby forming an electrode layer having a thickness of $1 \text{ }\mu\text{m}$. Thus, a multi-layered unit including the ceramic green sheet and the electrode layer laminated on the polyethylene terephthalate film was fabricated.

[0246]

The surface roughness (R_a) of the thus formed electrode layer was measured using the "SURFCORDER (SE-30D)" (Product Name) manufactured by Kosaka Laboratory Ltd. in the manner of Working Example 1. As a result, it was found that the surface roughness (R_a) of the electrode layer was $0.192 \text{ }\mu\text{m}$ and that since the surface roughness of the electrode layer was too high, the electrode layer having a high surface smoothness could not be formed.

[0247]

It was reasonable to conclude that this was because the viscosity of the conductive paste at the shearing velocity of 50 sec^{-1} was too high to print the conductive paste in a desired manner.

[0248]

Further, a total of fifty multi-layered ceramic capacitor samples were fabricated and the resistance value of each of the thus fabricated multi-layered ceramic capacitor samples was measured using a multi-meter in a manner of Working Example 1 to check whether or not short-circuit failure occurred therein. As a result, the short-circuit failure ratio of the multi-layered ceramic capacitor samples was found to be 40 % and it was found that the short-circuit failure was very high.

[0249]

Comparative Example 8

A conductive paste was prepared in the manner of Working Example 7 except that ethyl cellulose having a weight average molecular weight of 130,000 was used as a binder of a conductive paste and the viscosity of the thus prepared conductive paste was measured under conditions of a temperature of 25 °C and shearing velocity of 8 sec⁻¹ and was also measured under conditions of a temperature of 25 °C and shearing velocity of 50 sec⁻¹.

[0250]

As a result, it was found that the viscosity of the conductive paste measured under condition of the shearing velocity of 8 sec⁻¹ was 5.3 Ps·s and that the viscosity of the conductive paste measured under condition of the shearing velocity of 50 sec⁻¹ was 3.0 Ps·s.

[0251]

Then, the thus prepared conductive paste was printed on a ceramic green sheet fabricated in the manner of Working Example 1 using a screen printing machine, thereby forming an electrode layer having a thickness of 1 μm. Thus, a multi-layered unit including the ceramic green sheet and the electrode layer laminated on the polyethylene terephthalate film was fabricated.

[0252]

The surface roughness (Ra) of the thus formed electrode layer was measured using the "SURFCORDER (SE-30D)" (Product Name) manufactured by Kosaka Laboratory Ltd. in the manner of Working Example 1. As a result, it was found that the surface roughness (Ra) of the electrode layer was 0.071 μm and that the surface smoothness of the electrode layer was high. However, it was found that since the viscosity of

the conductive paste at the shearing velocity of 50 sec^{-1} was too low and the fluidity of the conductive paste was too high, the conductive paste leaked from a screen printing plate and the electrode layer could not be printed in a desired manner.

5 [0253]

Comparative Example 9

A dielectric paste for forming a ceramic green sheet was prepared in the manner of Working Example 1 except that butyral system resin whose degree of polymerization was 800 and degree of butyralization was
10 69 mol % was used as a binder of the dielectric paste for forming a ceramic green sheet, thereby forming a ceramic green sheet.

Further, a conductive paste was prepared in the manner of Working Example 8 and the viscosity of the thus prepared dielectric paste for forming a ceramic green sheet was measured under conditions of a
15 temperature of 25°C and shearing velocity of 8 sec^{-1} and was also measured under conditions of a temperature of 25°C and shearing velocity of 50 sec^{-1} .

[0254]

As a result, it was found that the viscosity of the conductive paste
20 measured under condition of the shearing velocity of 8 sec^{-1} was $11.7 \text{ Ps}\cdot\text{s}$ and that the viscosity of the conductive paste measured under condition of the shearing velocity of 50 sec^{-1} was $6.6 \text{ Ps}\cdot\text{s}$.

[0255]

Then, the thus prepared conductive paste was printed on a ceramic
25 green sheet fabricated in the manner of Working Example 1 using a screen printing machine, thereby forming an electrode layer having a thickness of $1 \mu\text{m}$. Thus, a multi-layered unit including the ceramic green sheet and the electrode layer laminated on the polyethylene terephthalate

film was fabricated.

[0256]

The surface roughness (Ra) of the thus formed electrode layer was measured using the "SURFCORDER (SE-30D)" (Product Name) manufactured by Kosaka Laboratory Ltd. in the manner of Working Example 1. As a result, it was found that the surface roughness (Ra) of the electrode layer was 0.091 μm and that the electrode layer having a high surface smoothness was formed.

[0257]

Further, a total of fifty multi-layered ceramic capacitor samples were fabricated and the resistance value of each of the thus fabricated multi-layered ceramic capacitor samples was measured using a multi-meter in a manner of Working Example 1 to check whether or not short-circuit failure occurred therein. As a result, the short-circuit failure ratio of the multi-layered ceramic capacitor samples was found to be 30 % and it was found that the short-circuit failure was so high that the samples were of no practical use.

[0258]

Comparative Example 10

A conductive paste was prepared in the manner of Comparative Example 2 except that a mixed solvent of terpineol and kerosene (mixture ratio (mass ratio) of 50:50) was used instead of isobornyl acetate as the solvent for preparing the conductive paste and the viscosity of the thus prepared conductive paste was measured under conditions of a temperature of 25 °C and shearing velocity of 8 sec^{-1} and was also measured under conditions of a temperature of 25 °C and shearing velocity of 50 sec^{-1} .

[0259]

As a result, it was found that the viscosity of the conductive paste measured under condition of the shearing velocity of 8 sec^{-1} was $10.7 \text{ Ps}\cdot\text{s}$ and that the viscosity of the conductive paste measured under condition of the shearing velocity of 50 sec^{-1} was $6.7 \text{ Ps}\cdot\text{s}$.

5 [0260]

Then, the thus prepared conductive paste was printed on a ceramic green sheet fabricated in the manner of Working Example 1 using a screen printing machine, thereby forming an electrode layer having a thickness of $1 \text{ }\mu\text{m}$. Thus, a multi-layered unit including the ceramic green
10 sheet and the electrode layer laminated on the polyethylene terephthalate film was fabricated.

[0261]

The surface roughness (Ra) of the thus formed electrode layer was measured using the "SURFCORDER (SE-30D)" (Product Name)
15 manufactured by Kosaka Laboratory Ltd. in the manner of Working Example 1. As a result, it was found that the surface roughness (Ra) of the electrode layer was $0.129 \text{ }\mu\text{m}$ and that the electrode layer having a high surface smoothness was formed.

[0262]

20 Further, a total of fifty multi-layered ceramic capacitor samples were fabricated and the resistance value of each of the thus fabricated multi-layered ceramic capacitor samples was measured using a multi-meter in a manner of Working Example 1 to check whether or not short-circuit failure occurred therein. As a result, the short-circuit failure
25 ratio of the multi-layered ceramic capacitor samples was found to be 76 % and it was found that the short-circuit failure was so high that the samples were of no practical use.

[0263]

It is reasonable to conclude that this was because the mixed solvent of terpineol and kerosene used as a solvent of the conductive paste dissolved a copolymer of methyl methacrylate and butyl acrylate used as the binder of the ceramic green sheet.

5 [0264]

Comparative Example 11

A conductive paste was prepared in the manner of Comparative Example 2 except that terpineol was used instead of isobornyl acetate as the solvent for preparing the conductive paste and the viscosity of the
10 thus prepared conductive paste was measured under conditions of a temperature of 25 °C and shearing velocity of 8 sec⁻¹ and was also measured under conditions of a temperature of 25 °C and shearing velocity of 50 sec⁻¹.

[0265]

15 As a result, it was found that the viscosity of the conductive paste measured under condition of the shearing velocity of 8 sec⁻¹ was 13.1 Ps·s and that the viscosity of the conductive paste measured under condition of the shearing velocity of 50 sec⁻¹ was 6.9 Ps·s.

[0266]

20 Then, the thus prepared conductive paste was printed on a ceramic green sheet fabricated in the manner of Working Example 1 using a screen printing machine, thereby forming an electrode layer having a thickness of 1 μm. Thus, a multi-layered unit including the ceramic green sheet and the electrode layer laminated on the polyethylene terephthalate
25 film was fabricated.

[0267]

The surface roughness (Ra) of the thus formed electrode layer was measured using the "SURFCORDER (SE-30D)" (Product Name)

manufactured by Kosaka Laboratory Ltd. in the manner of Working Example 1. As a result, it was found that the surface roughness (Ra) of the electrode layer was 0.192 μm and that since the surface roughness of the electrode layer was too high, the electrode layer having a high surface smoothness could not be formed.

[0268]

It is reasonable to conclude that this was because terpeneol used as a solvent of the conductive paste dissolved a copolymer of methyl methacrylate and butyl acrylate used as the binder of the ceramic green sheet.

[0269]

Further, a total of fifty multi-layered ceramic capacitor samples were fabricated and the resistance value of each of the thus fabricated multi-layered ceramic capacitor samples was measured using a multi-meter in a manner of Working Example 1 to check whether or not short-circuit failure occurred therein. As a result, the short-circuit failure ratio of the multi-layered ceramic capacitor samples was found to be 88 % and it was found that the short-circuit failure was so high that the samples were of no practical use.

[0270]

It is reasonable to conclude that this was because terpeneol used as a solvent of the conductive paste dissolved a copolymer of methyl methacrylate and butyl acrylate used as the binder of the ceramic green sheet.

[0271]

Comparative Example 12

A conductive paste was prepared in the manner of Comparative Example 2 except that dihydroterpeneol was used instead of isobornyl

acetate as the solvent for preparing the conductive paste and the viscosity of the thus prepared conductive paste was measured under conditions of a temperature of 25 °C and shearing velocity of 8 sec⁻¹ and was also measured under conditions of a temperature of 25 °C and shearing
5 velocity of 50 sec⁻¹.

[0272]

As a result, it was found that the viscosity of the conductive paste measured under condition of the shearing velocity of 8 sec⁻¹ was 13.4 Ps·s and that the viscosity of the conductive paste measured under condition of
10 the shearing velocity of 50 sec⁻¹ was 6.8 Ps·s.

[0273]

Then, the thus prepared conductive paste was printed on a ceramic green sheet fabricated in the manner of Working Example 1 using a screen printing machine, thereby forming an electrode layer having a
15 thickness of 1 µm. Thus, a multi-layered unit including the ceramic green sheet and the electrode layer laminated on the polyethylene terephthalate film was fabricated.

[0274]

The surface roughness (Ra) of the thus formed electrode layer was
20 measured using the "SURFCORDER (SE-30D)" (Product Name) manufactured by Kosaka Laboratory Ltd. in the manner of Working Example 1. As a result, it was found that the surface roughness (Ra) of the electrode layer was 0.129 µm and that the electrode layer having a high surface smoothness was formed.

25 [0275]

Further, a total of fifty multi-layered ceramic capacitor samples were fabricated and the resistance value of each of the thus fabricated multi-layered ceramic capacitor samples was measured using a

multi-meter in the manner of Working Example 1 to check whether or not short-circuit failure occurred therein. As a result, the short-circuit failure ratio of the multi-layered ceramic capacitor samples was found to be 56 % and it was found that the short-circuit failure was so high that the samples were of no practical use.

[0276]

It is reasonable to conclude that this was because dihydroterpineol used as a solvent of the conductive paste dissolved a copolymer of methyl methacrylate and butyl acrylate used as the binder of the ceramic green sheet.

[0277]

It was found from Working Examples 1 to 15 and Comparative Examples 10 to 12 that in the case where the conductive paste containing ethyl cellulose having a weight average molecular weight of 130,000 as a binder and the mixed solvent of terpineol and kerosene (mixture ratio (mass ratio) of 50:50) as a solvent, the conductive paste containing ethyl cellulose having a weight average molecular weight of 130,000 as a binder and terpineol as a solvent or the conductive paste containing ethyl cellulose having a weight average molecular weight of 130,000 as a binder and dihydroterpineol as a solvent was printed on the ceramic green sheet formed by using the dielectric paste containing polyvinyl butyral whose degree of polymerization was 1450 and degree of butyralization was 69 mol % as a binder, thereby fabricating the multi-layered unit, and the fifty multi-layered units were laminated, thereby fabricating the multi-layered ceramic capacitor, the solvent of the conductive paste dissolved polyvinyl butyral contained in the ceramic green sheet as a binder, so that the ceramic green sheet was swollen or partially dissolved, thereby generating pinholes or cracks in the ceramic green sheet and

causing the short-circuit failure ratio of the multi-layered ceramic capacitors to become extremely high, while in the case where the conductive paste containing ethyl cellulose having an apparent weight average molecular weight of 155,000 to 205,000 defined by $X * MW_L + (1-X) * MW_H$ as a binder and isobornyl acetate, dihydroterpinyl methyl ether, terpinyl methyl ether, α -terpinyl acetate, I-dihydrocarvyl acetate, I-menthone, I-menthyl acetate, I-perillyl acetate or I-carvyl acetate as a solvent was printed on the ceramic green sheet formed by using the dielectric paste containing polyvinyl butyral whose degree of polymerization was 1450 and degree of butyralization was 69 mol % as a binder, thereby fabricating the multi-layered unit, and the fifty multi-layered units were laminated, thereby fabricating the multi-layered ceramic capacitor, the solvent of the conductive paste hardly dissolved polyvinyl butyral contained in the ceramic green sheet as a binder, so that the ceramic green sheet was not swollen or partially dissolved, thereby preventing generation of pinholes or cracks in the ceramic green sheet and markedly decreasing the short-circuit failure ratio of the multi-layered ceramic capacitors.

[0278]

Further, it was found from Working Examples 1 to 15 and Comparative Examples 1, 4 and 7 that in the case where the conductive paste containing ethyl cellulose having a weight average molecular weight of 230,000 as a binder and isobornyl acetate as a solvent, the conductive paste containing ethyl cellulose having a weight average molecular weight of 230,000 as a binder and dihydroterpinyl methyl ether as a solvent or the conductive paste containing ethyl cellulose having a weight average molecular weight of 230,000 as a binder and terpinyl methyl ether as a solvent was printed on the ceramic green sheet formed

by using the dielectric paste containing polyvinyl butyral whose degree of polymerization was 1450 and degree of butyralization was 69 mol % as a binder, thereby fabricating the multi-layered unit, and the fifty multi-layered units were laminated, thereby fabricating the multi-layered ceramic capacitor, the viscosity of the conductive paste was so high that it was impossible to print the conductive paste on the ceramic green sheet in a desired manner to form the electric layer having a high surface smoothness, so that the short-circuit failure ratio of the multi-layered ceramic capacitors became extremely high, while in the case where the conductive paste containing ethyl cellulose having an apparent weight average molecular weight of 155,000 to 205,000 defined by $X \cdot MW_L + (1-X) \cdot MW_H$ as a binder and isobornyl acetate, dihydroterpinyl methyl ether, terpinyl methyl ether, α -terpinyl acetate, I-dihydrocarvyl acetate, I-menthone, I-menthyl acetate, I-perillyl acetate or I-carvyl acetate as a solvent was printed on the ceramic green sheet formed by using the dielectric paste containing polyvinyl butyral whose degree of polymerization was 1450 and degree of butyralization was 69 mol % as a binder, thereby fabricating the multi-layered unit, and the fifty multi-layered units were laminated, thereby fabricating the multi-layered ceramic capacitor, the conductive paste had a viscosity suitable for printing, so that it was possible to form an electric layer on a ceramic green sheet in a predetermined pattern using a screen printing machine in a desired manner and fabricate the multi-layered ceramic capacitors whose short-circuit failure ratio was low.

[0279]

Furthermore, it was found from Working Examples 1 to 15 and Comparative Examples 2, 5 and 8 that in the case where the conductive paste containing ethyl cellulose having a weight average molecular

weight of 130,000 as a binder and isobornyl acetate as a solvent, the
conductive paste containing ethyl cellulose having a weight average
molecular weight of 130,000 as a binder and dihydroterpinyl methyl ether
as a solvent or the conductive paste containing ethyl cellulose having a
weight average molecular weight of 130,000 as a binder and terpinyl
methyl ether as a solvent was printed on the ceramic green sheet formed
by using the dielectric paste containing polyvinyl butyral whose degree of
polymerization was 1450 and degree of butyralization was 69 mol % as a
binder, thereby fabricating the multi-layered unit, the viscosity of the
conductive paste was too low and the fluidity of the conductive paste was
too high, so that the conductive paste leaked from a screen printing plate
and the electrode layer could not be formed in a desired pattern, while in
the case where the conductive paste containing ethyl cellulose having an
apparent weight average molecular weight of 155,000 to 205,000 defined
by $X \cdot MW_L + (1-X) \cdot MW_H$ as a binder and isobornyl acetate,
dihydroterpinyl methyl ether, terpinyl methyl ether, α -terpinyl acetate,
I-dihydrocarvyl acetate, I-menthone, I-menthyl acetate, I-perillyl acetate
or I-carvyl acetate as a solvent was printed on the ceramic green sheet
formed by using the dielectric paste containing polyvinyl butyral whose
degree of polymerization was 1450 and degree of butyralization was 69
mol % as a binder, thereby fabricating the multi-layered unit, and the
fifty multi-layered units were laminated, thereby fabricating the
multi-layered ceramic capacitor, the conductive paste had a viscosity
suitable for printing, so that it was possible to form an electric layer on a
ceramic green sheet in a predetermined pattern using a screen printing
machine in a desired manner and fabricate the multi-layered ceramic
capacitors whose short-circuit failure ratio was low.

[0280]

Moreover, it was found from Working Examples 1 to 15 and Comparative Examples 3, 6 and 9 that in the case where the conductive paste containing ethyl cellulose having an apparent weight average molecular weight of 180,000 as a binder and isobornyl acetate as a solvent, the conductive paste containing ethyl cellulose having an apparent weight average molecular weight of 180,000 as a binder and dihydroterpinyl methyl ether as a solvent or the conductive paste containing ethyl cellulose having an apparent weight average molecular weight of 180,000 as a binder and terpinyl methyl ether as a solvent was printed on the ceramic green sheet formed by using the dielectric paste containing polyvinyl butyral whose degree of polymerization was 1450 and degree of butyralization was 69 mol % as a binder, thereby fabricating the multi-layered unit, the short-circuit failure ratio of the multi-layered ceramic capacitors became very high, while in the case where the conductive paste containing ethyl cellulose having an apparent weight average molecular weight of 155,000 to 205,000 defined by $X \cdot MW_L + (1-X) \cdot MW_H$ as a binder and isobornyl acetate, dihydroterpinyl methyl ether, terpinyl methyl ether, α -terpinyl acetate, I-dihydrocarvyl acetate, I-menthone, I-menthyl acetate, I-perillyl acetate or I-carvyl acetate as a solvent was printed on the ceramic green sheet formed by using the dielectric paste containing polyvinyl butyral whose degree of polymerization was 1450 and degree of butyralization was 69 mol % as a binder, thereby fabricating the multi-layered unit, and the fifty multi-layered units were laminated, thereby fabricating the multi-layered ceramic capacitor, the solvent of the conductive paste hardly dissolved polyvinyl butyral contained in the ceramic green sheet as a binder, so that it was possible to prevent the ceramic green sheet being swollen or partially dissolved, thereby preventing generation of pinholes or cracks in

the ceramic green sheet and markedly decreasing the short-circuit failure ratio of the multi-layered ceramic capacitors.

[0281]

Further, it was found that in the case where a dielectric paste
5 adapted for forming a spacer layer and containing ethyl cellulose having an apparent weight average molecular weight of 110,000 to 180,000 defined by $X \cdot MW_L + (1-X) \cdot MW_H$ as a binder and isobornyl acetate, dihydroterpinyl methyl ether, terpinyl methyl ether, α -terpinyl acetate, I-dihydrocarvyl acetate, I-menthone, I-menthyl acetate, I-perillyl acetate
10 or I-carvyl acetate as a solvent was prepared and the dielectric paste was printed on the ceramic green sheet in a complimentary pattern to that of the electrode layer, thereby forming a spacer layer, the same results as those above were obtained.

[0282]

15 The present invention has thus been shown and described with reference to the preferred embodiments and the working examples. However, it should be noted that the present invention is in no way limited to the details of the described arrangement but changes and modifications may be made without departing from the scope of the
20 appended claims.

[0283]

According to the present invention, it is possible to provide a conductive paste for a multi-layered ceramic electronic component which does not dissolve a binder contained in a layer adjacent to an electrode
25 layer of the multi-layered ceramic electronic component, can reliably prevent short circuit failure from occurring in a multi-layered ceramic electronic component and has excellent printability.

[0284]

Further, according to the present invention, it is possible to provide a method for manufacturing a multi-layered unit for a multi-layered ceramic electronic component which can reliably prevent short circuit failure from occurring in a multi-layered ceramic electronic
5 component and form an electrode layer in a desired manner.